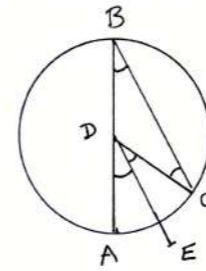


# Axial Magnification

Gregg Baldwin, OD  
2022

1



$$\angle ADC = 2 \angle ABC$$

$$\angle ADC = \angle FDC - \angle FDA, \text{ or:}$$

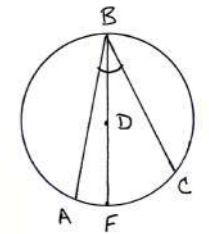
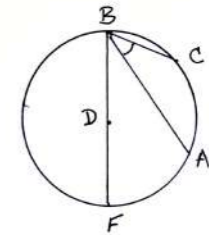
$$\angle ADC = \angle FDC + \angle FDA$$

$$\angle ADC = 2(\angle FBC \text{ +/- } \angle FBA)$$

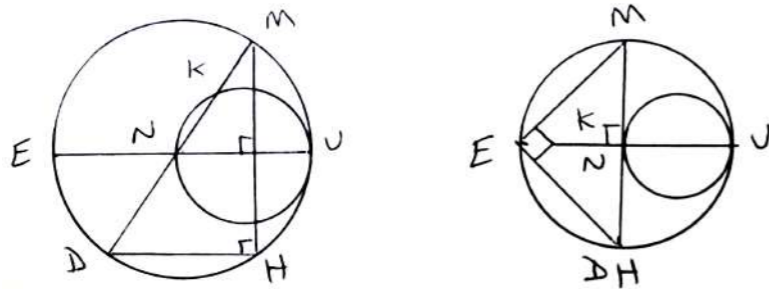
$$\angle ADC = 2 \angle ABC$$

Therefore  $\angle ABC$  can be defined as:

$$\sim AC/BF, \text{ or } 1/2(\sim AC/DF).$$



2



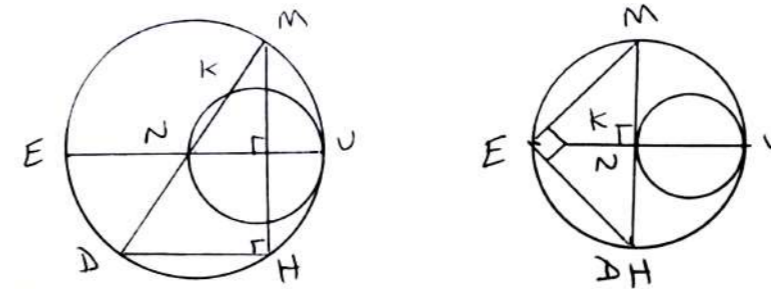
$$2 \sim KU/UN = 2 \angle MNU = \angle MNH$$

$$\text{As } K \Rightarrow N \text{ and } D \Rightarrow H, \quad 2 \sim KU/UN \Rightarrow \pi$$

$$\angle ABC + \angle BCA + \angle CAB = \sim CA/BF + \sim AB/BF + \sim BC/BF = \pi$$

If two angles of two triangles are the same, their third angles are the same. They are consequently the same shape, (are  $\cong$ ), with equal side ratios.

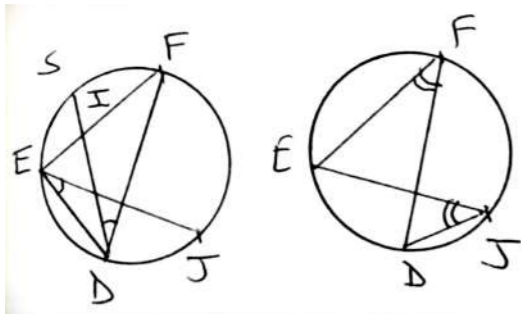
3



$$\sim UK/UN = \sim MH/MD = 2 \sim UM/UE = 2 \sim UM/2UN$$

$$\sim UK = \sim UM$$

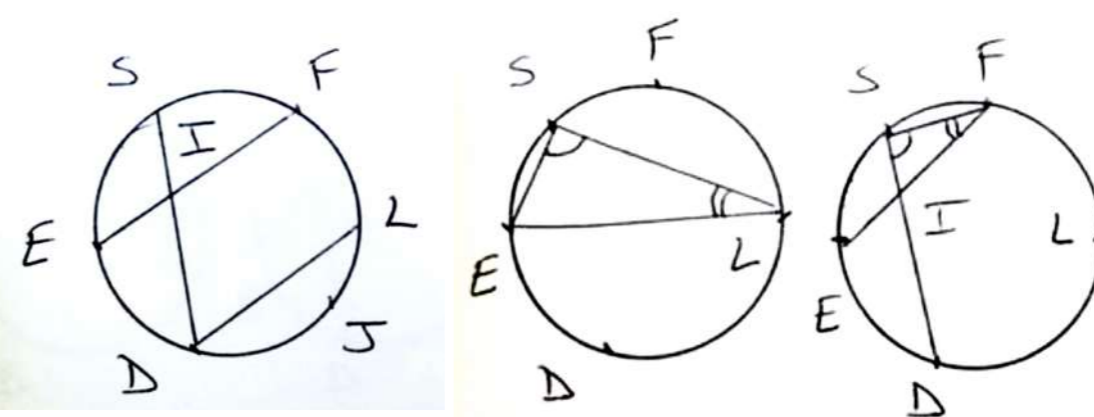
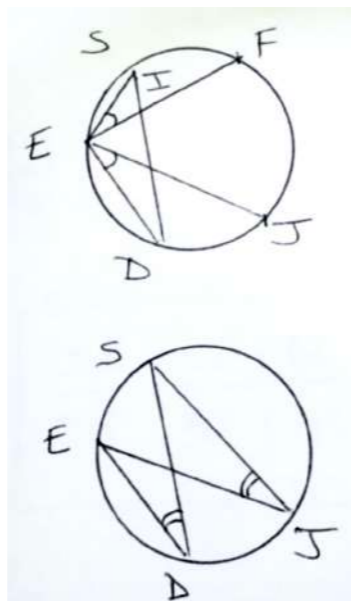
4



$SD \parallel FJ$   
 $\triangle EJD \cong \triangle DFI$ ;  $FD/FI = JE/JD$   
 $\triangle EJS \cong \triangle EDI$ ;  $EI/ED = ES/EJ$   
 $[(FD)(EI)]/[(FI)(ED)]$   
 $= [(JE)(ES)]/[(JD)(EJ)] = SE/SF$

**$IE/IF = [(SE)(DE)]/[(SF)(DF)]$**

5



$LD \parallel FE$  ;  $DE/DF = LF/LE$ ;  $IE/IF = (SE)(LF)/(SF)(LE)$   
 $FE/FI = \{(SE)(LF) + (SF)(LE)\}/(SF)(LE)$   
 $LD \parallel FE$ ;  $\sim EL = \sim FD$   
 $\triangle LSE \cong \triangle FSI$ ;  $LS/FS = LE/FI$ ;  $LS = \{(FS)(LE)\}/FI$

**Ptolemy's Theorem:**

**$(FE)(LS) = (SE)(LF) + (SF)(LE)$**

6

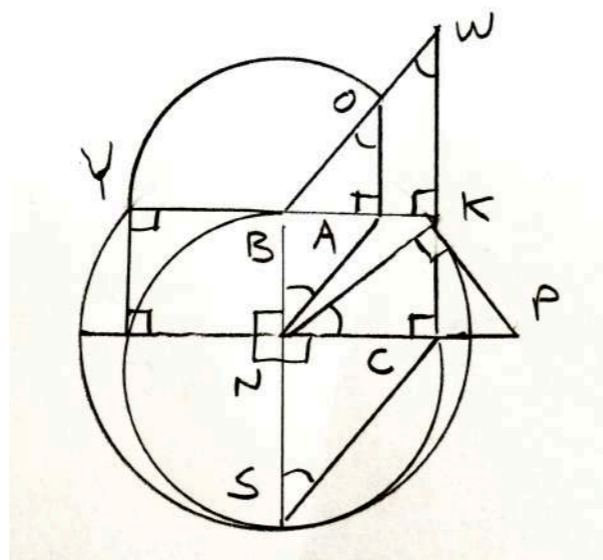
$NS/NC = NC/NB$   
 $NK/NC = CN/CK$

$\triangle NSC = \triangle KWB =$   
 $\triangle KNP$   
 $NC = KP$

$\triangle CKP = \triangle BNA = \triangle AOB$   
 $NA = KP$

$NC = NA = OB$   
 $NC = KB = YB$

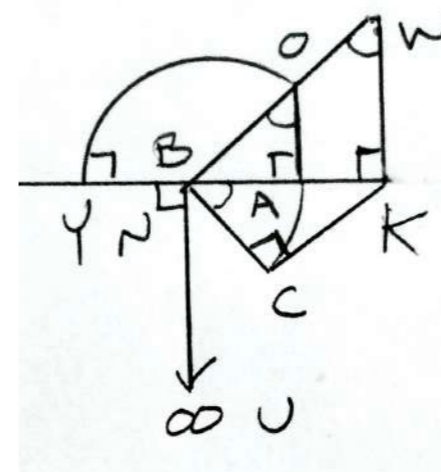
$WK = NS = YN$



7

Keeping only:

$NA = NC$ , and  $\triangle CNK \cong \triangle AOB \cong \triangle KWB$ :



As  $N \Rightarrow B$ ,  $WK \Rightarrow YN$

because:

$WK/OA \Rightarrow NK/NA$

$= NK/NC$

$= OB/OA$

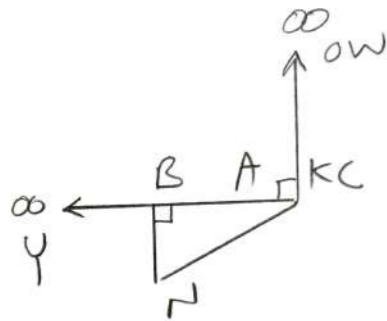
$= WB/WK$

so that:

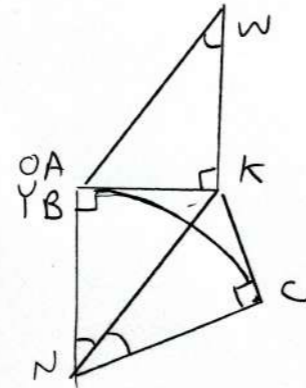
$WK \Rightarrow OB \Rightarrow YN$

8

Keeping only:  
 $NA = NC$ , and  $\Delta CNK \cong \Delta AOB \cong \Delta KWB$ :

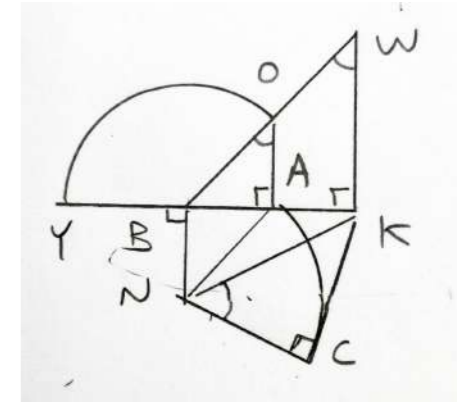


As  $A \Rightarrow K$ ,  $WK \Rightarrow YN$

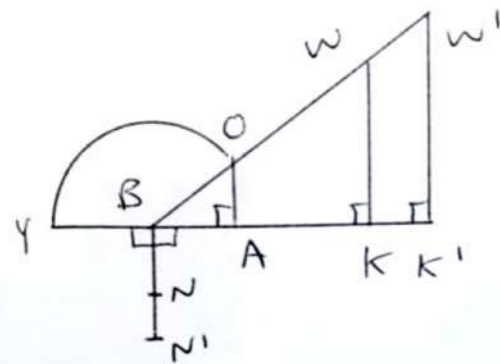


As  $A \Rightarrow B$ ,  $WK \Rightarrow YN$

Therefore,  
 whenever A lies on KB of  
 right triangle  $\Delta KBN$ ;  
 if  $NA = NC$ , and  
 $\Delta CNK \cong \Delta AOB \cong \Delta KWB$ ,  
 then  $WK = YN$



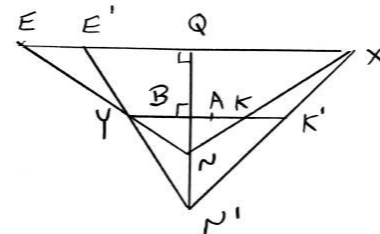
which also can be shown directly, using the equations:  
 $(CK/CN)^2 = (AB/AO)^2 = (KB/KW)^2 = (CK^2 + AB^2)/(CN^2 + AO^2)$   
 since:  $KB^2 = KN^2 - BN^2 = KN^2 - (NC^2 - AB^2) = CK^2 + AB^2$   
 then:  $WK^2 = CN^2 + AO^2$ , which equals:  
 $AN^2 + AO^2 = BA^2 + BN^2 + BO^2 - BA^2 = YN^2$



$OB/OA = NK/NA = N'K'/N'A$

$KW = YN$   
 $K'W' = YN'$

$KB/YN = K'B/YN'$



$QX/EN = KB/YN$   
 $= K'B/YN' = QX/E'N'$

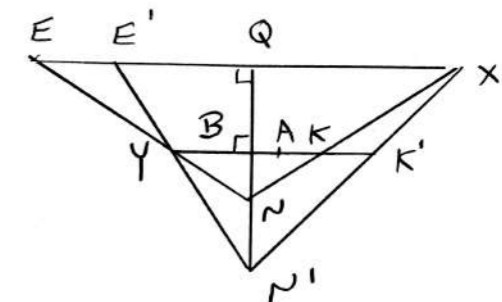
$EN = E'N'$

Only one  $N'K'X$   
 exists for  $NKX$  since  
 only one  $E'N'$  exists  
 equal to  $EN$ .

When  $EN$  is changed to become the smallest  
 segment through  $Y$ ,  
 bound by the right angle  $EQN$ :

$E'$  lies at  $E$ , and  
 $N'$  lies at  $N$ .

Also,  $QX$  varies with  
 $EN$  because:  
 $QX/EN = KB/YN$   
 $= KB/KW$ , which is a  
 constant.

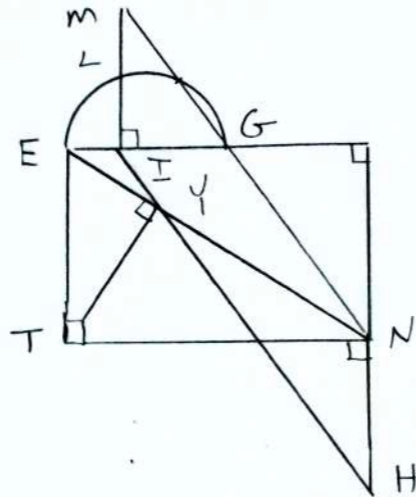


To specify EN as the shortest hypotenuse through Y:

NE || GL  
 TY || EL  
 HI || NM  
 HI = NM > NL

NL is the hypotenuse of right triangle NEL, so:

NL > NE  
 HI > NE



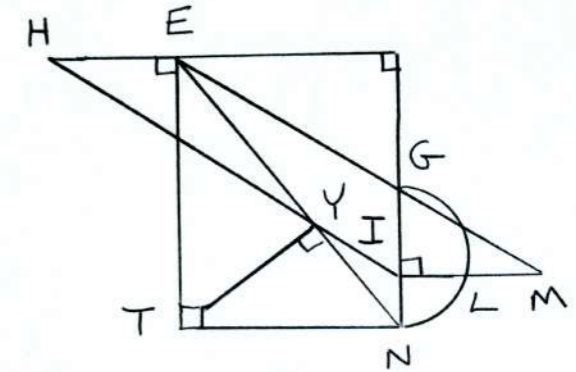
13

But also:

NE || GL  
 TY || NL  
 HI || EM  
 HI = EM > EL

EL is the hypotenuse of right triangle ENL, so:

EL > EN  
 HI > EN

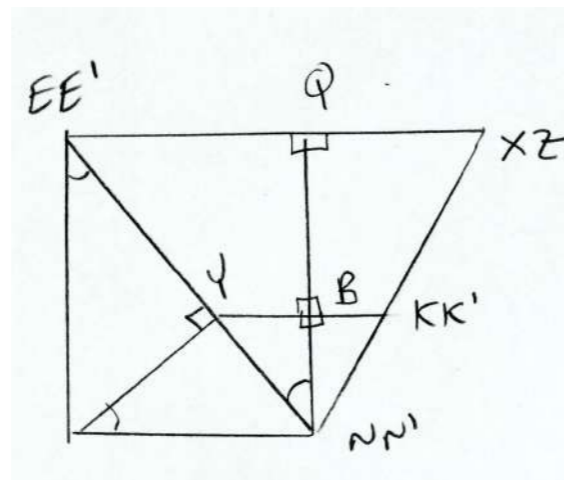


14

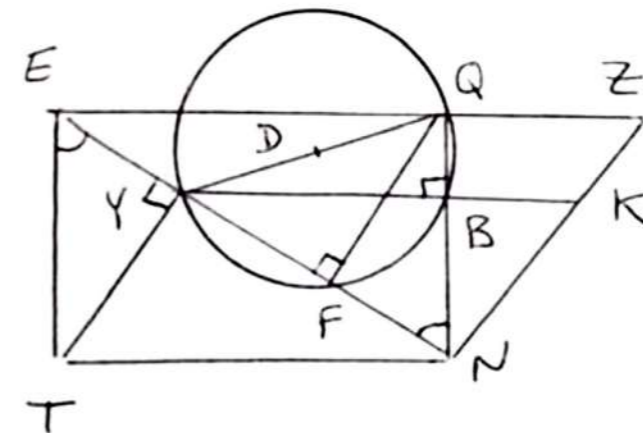
Let X = Z when EN is the shortest segment through Y included in right angle EQN.

In order to find Z given  $\Delta YBN$ , we must find  $E = E'$  using:

$$\Delta YBN \cong \Delta NYT \cong \Delta NTE$$



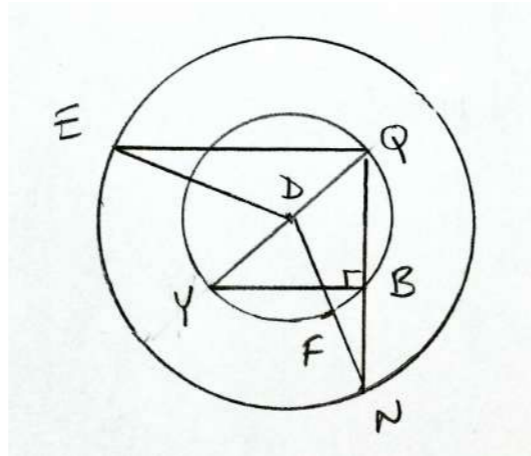
15



In order to find Z given  $\Delta YBQ$ , we must find  $EN = E'N'$  by making  $\Delta TYE$  a right triangle.

16

Draw a concentric circle around  $\odot YBQ$  using its center at D, (the midpoint of hypotenuse YQ), containing an arc  $\sim EN$ , so that YF lies on its chord EN. The arc intercepted by  $\angle DEN$  then equals that intercepted by  $\angle DNE$ .



17

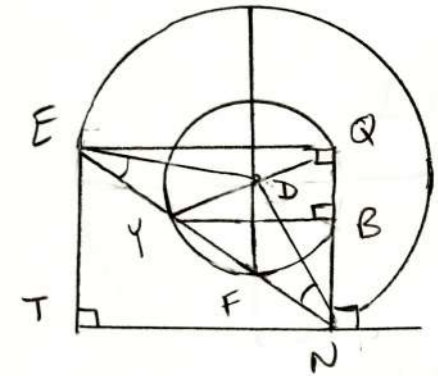
$$\angle DEY = \angle DNF$$

$$DY = DF ; DE = DN$$

$$\triangle EDY = \triangle NDF$$

$$EY = NF$$

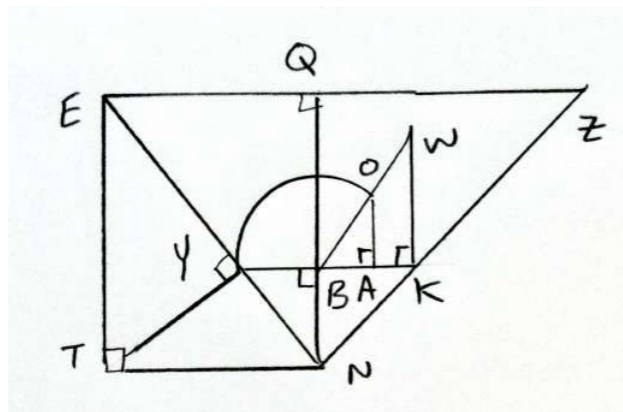
Since  $\triangle QFN$  is a right triangle, so is  $\triangle TYE$ .



18

$$WK = YN$$

Given  $\triangle BAO$ :



use  $\triangle BNY$  to find  $\triangle BKW$  and  $\triangle QBY$ ,

use  $\triangle QBY$  or  $\triangle BKW$  to find  $\triangle BNY$ .

19

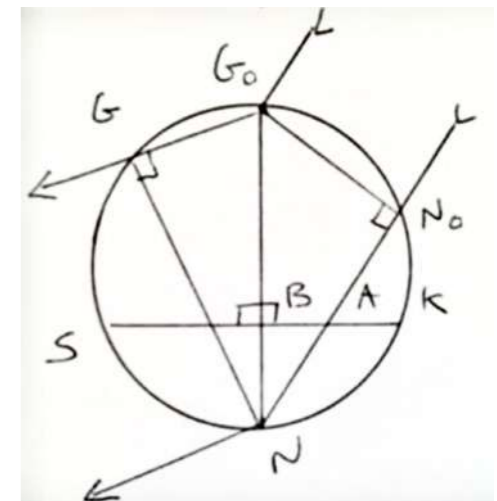
$$\triangle N_oNK \cong \triangle KNA$$

because:

$$\sim NS = \sim NK$$

across diameter  $G_oN$ .

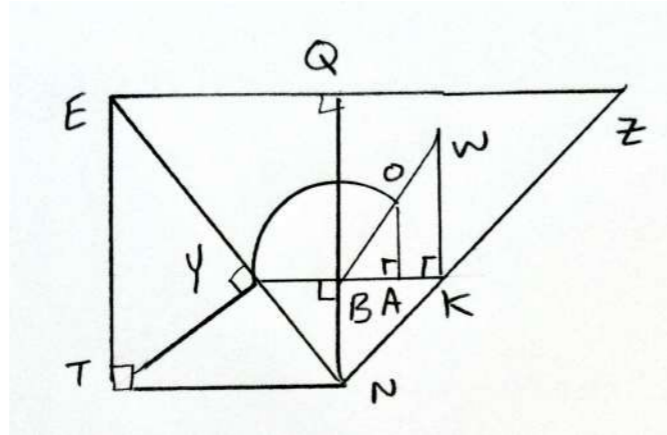
Wavefront  $G_oN_o$  refracts into wavefront  $GN$  along  $G_oN$ , since it travels  $G_oG$  in the same time it travels  $N_oN$ .



$$\mathbb{R} = NN_o/GG_o = NN_o/NK = NK/NA$$

20

Therefore, if  $\mathbb{R} = OB/OA$ , and  $WK = YN$ ; then,  $\mathbb{R} = NK/NA$



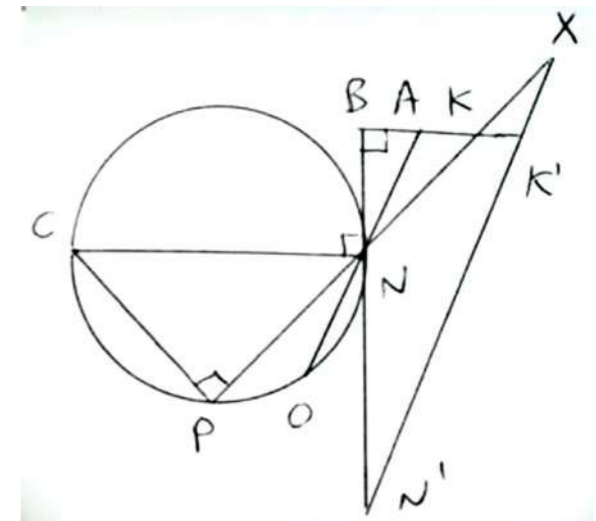
and Z is the clear image of object A refracted at N (= N'), along BN, because the two possible refracted rays through Z coincide at N.

$$\Delta KNA \cong \Delta OCP$$

$$\mathbb{R} = NK/NA$$

$$= N'K'/N'A$$

$$= CO/CP$$



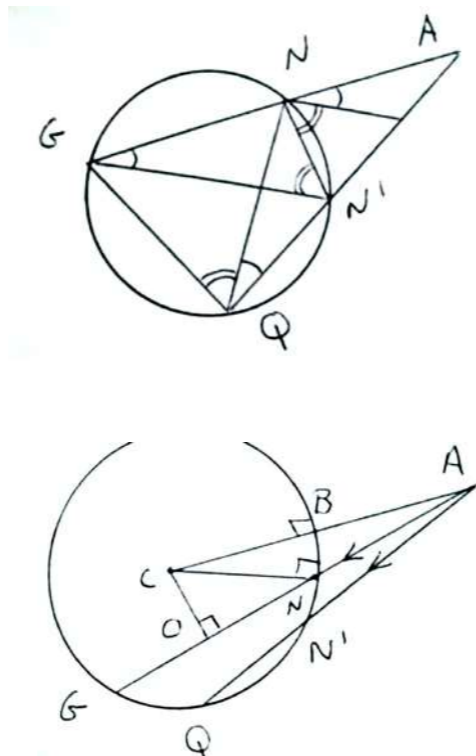
Real object A:

$$\Delta ANN' \cong \Delta AQQ$$

$$AG/AN' = QG/NN'$$

$$(AG + AN')/2AN'$$

$$= (QG + NN')/2NN'$$



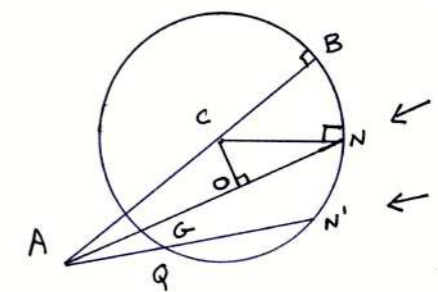
Virtual object A, which can not be projected on a screen due to refraction at BN:

$$\Delta ANN' \cong \Delta AQQ$$

$$AG/AN' = QG/NN'$$

$$(AG + AN')/2AN'$$

$$= (QG + NN')/2NN'$$



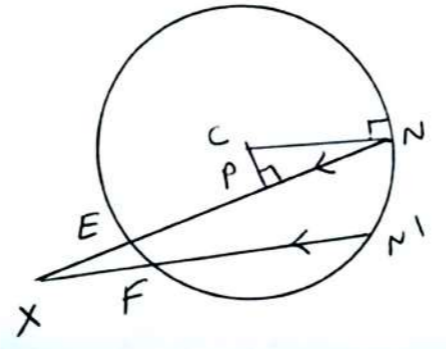
Real image at X,  
 (will be defined as clear  
 as  $N' \Rightarrow N$ , and  $X \Rightarrow Z$ ),  
 can be projected on a  
 screen:

$$\Delta XNN' \cong \Delta XFE$$

$$XE/XN' = EF/NN'$$

$$(XE + XN')/2XN'$$

$$= (EF + NN')/2NN'$$



25

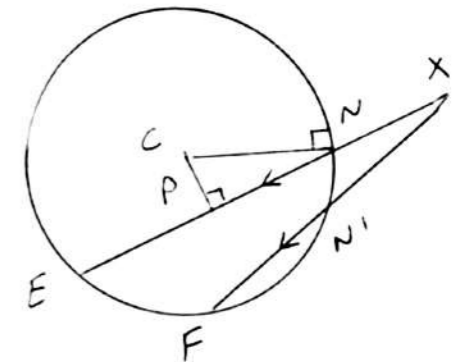
Virtual image at X,  
 (will be defined as clear  
 as  $N' \Rightarrow N$ , and  $X \Rightarrow Z$ ),  
 can not be projected on  
 a screen:

$$\Delta XNN' \cong \Delta XFE$$

$$XE/XN' = EF/NN'$$

$$(XE + XN')/2XN'$$

$$= (EF + NN')/2NN'$$



26

$$(AG + AN')/2AN' = (QG + NN')/2NN'$$

$$(XE + XN')/2XN' = (EF + NN')/2NN'$$

$$(QG + NN')/(EF + NN')$$

$$= [(AG + AN')/2AN'] [2XN'/(XE + XN')]$$

As  $N' \Rightarrow N$ ,  $X \Rightarrow Z$ , and:

$$(\sim QG + \sim NN')/(\sim EF + \sim NN')$$

$$\Rightarrow (QG + NN')/(EF + NN')$$

$$\Rightarrow (AO/AN)(ZN/ZP)$$

27

Also, when  $HD = QN'$   
 and  $RJ = FN'$

$$(\sim QG + \sim NN')/(\sim EF + \sim NN')$$

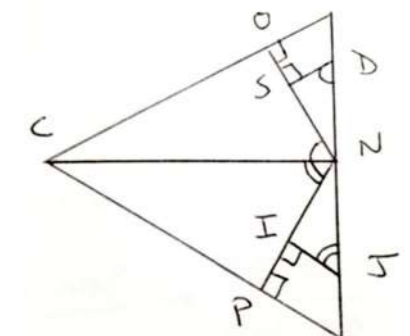
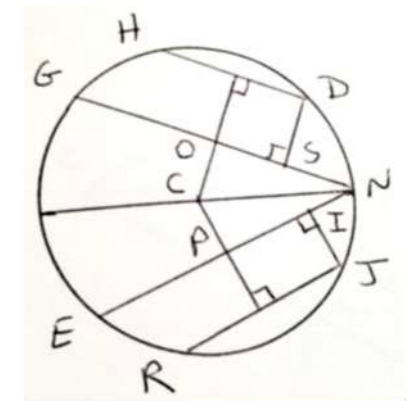
$$= 2(\sim ND)/2(\sim NJ) = \sim ND/\sim NJ$$

As  $N' \Rightarrow N$ ,  $X \Rightarrow Z$ , and:

$\sim DJ \Rightarrow$  line segment DJ, so:

$$(\sim QG + \sim NN')/(\sim EF + \sim NN')$$

$$\Rightarrow ND/NJ$$



28

$$\begin{aligned}
 DS/JI &= CO/CP \\
 JI/JN &= NP/NC \\
 DN/DS &= NC/NO \\
 ND/NJ &= (NP/NO)(CO/CP)
 \end{aligned}$$

As  $N' \Rightarrow N$ ,  $X \Rightarrow Z$ , and:

$$\begin{aligned}
 (\sim QG + \sim NN') / (\sim EF + \sim NN') \\
 \Rightarrow (NP/NO)(CO/CP)
 \end{aligned}$$

and therefore:

$$(AO/AN)(ZN/ZP) \Rightarrow (NP/NO)(CO/CP)$$

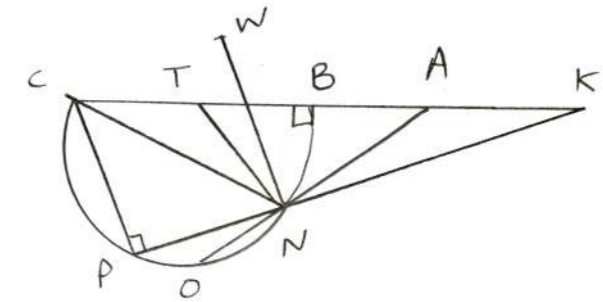
29

Thus  $R = CO/CP$ , and  $Z$ , (along both  $NP$  and  $CW$ ), is the clear image of  $A$  refracted along  $\sim BN$ , when:

$NT \parallel CO$ , so:  
 $AO/AN = CO/NT$  and:

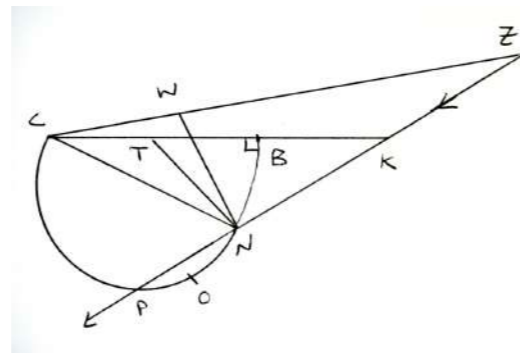
$NW \parallel CP$ , so:  
 $ZN/ZP = NW/CP$   
 and:

$NW/NT = NP/NO$   
 $(\Delta WNT \cong \Delta PNO)$



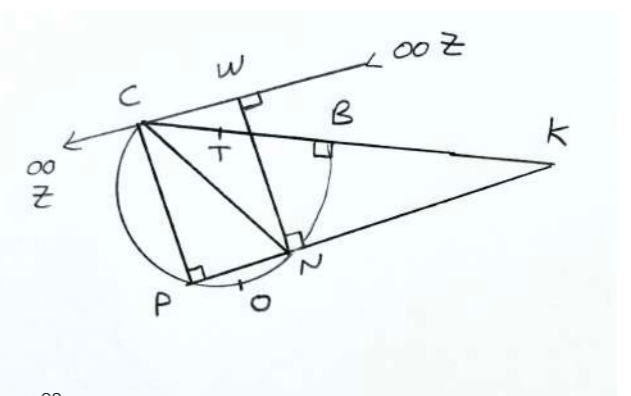
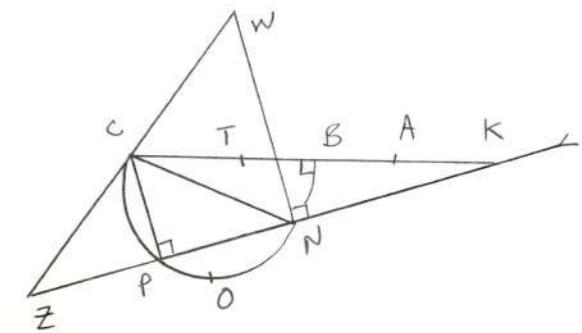
30

The off-axis rays from any on-axis object  $A$ , (real or virtual), can not form a virtual on-axis image at  $Z$  because  $NW$  must be less than  $CP$  for  $Z$  to be virtual; but  $NW$  must also be greater than  $NT$ .



31

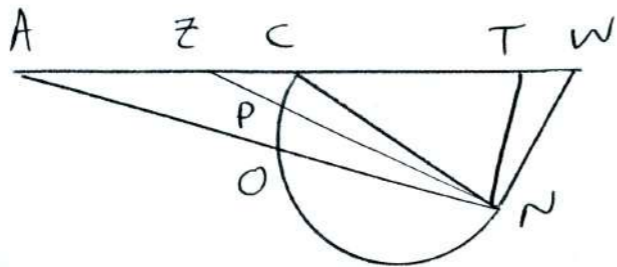
The off-axis rays from any real on-axis object  $A$  can not form a real on-axis image at  $Z$  because  $NW$  must be greater than (or equal to)  $CP$  for  $Z$  to be real; but  $NW$  must also be greater than  $NT$ .



32



The off-axis rays from a virtual on-axis object  $A$  can form a real on-axis image at  $Z$ , if  $NW$  is greater than  $CP$ , and  $WT$  lies along the axis.



33

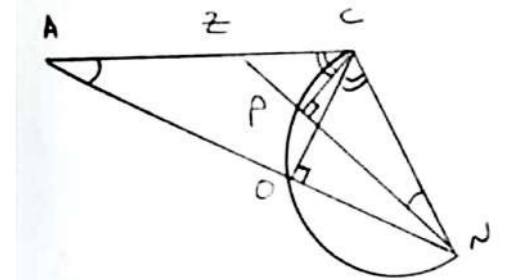
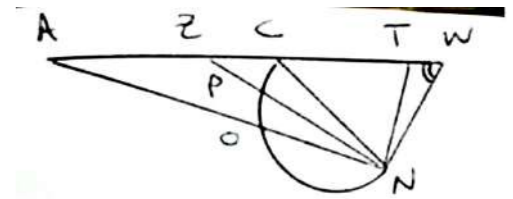
Since:

$$\angle NWT = \angle NPO = \angle NCO$$

and  $NW \parallel CP$

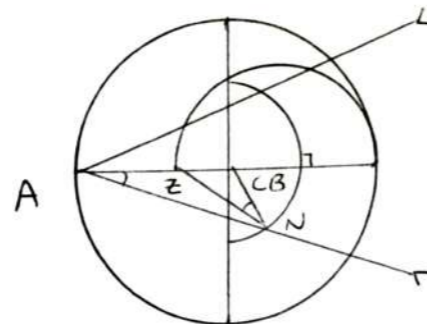
$WT$  lies along the axis when:

$$\triangle NCO \cong \triangle ZCP$$



34

When off-axis rays from a virtual on-axis object  $A$  form a real on-axis image  $Z$ , this occurs at all points  $N$  because:



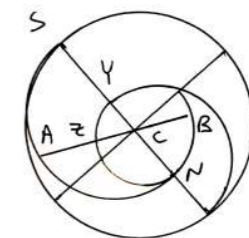
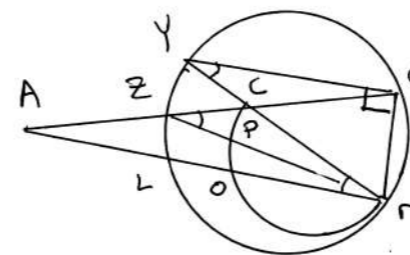
$\triangle ACN \cong \triangle NCZ$  for all  $N$ ,  
(since they share proportional sides around a common angle).

35

This can also be demonstrated using similar right triangles:  
 $\triangle SAN \cong \triangle CON$ , and  $\triangle YZN \cong \triangle CPN$ ,  
so that:  $(AO/AN)(ZN/ZP) = (SC/SN)(YN/YC)$ .

Since:  $CY/CN = CN/CS = (CY + CN)/(CN + CS) = NY/NS$   
 $(SC/SN) = (NC/NY)$ , and:

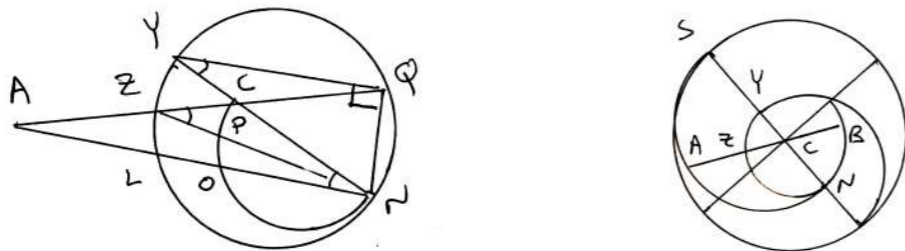
$$(AO/AN)(ZN/ZP) = CN/CY$$



36

But it is also true that:  
 $(CO/CP)(NP/NO) = CN/CY$ , because:

$(CO/CP)(NP/NO) = (LY/LN)(PN/PC) =$   
 $= (QN/QY)(PN/PC) = (QN/QY)(ZN/ZY) =$   
 $QN (ZN)/QY(ZY)$  which, by the property of cyclic  
 quadrilaterals discussed in slide #5, equals  $CN/CY$



37

Keeping:

$$\mathbb{R} = (CO/CP) = (NO/NP)(AO/AN)(ZN/ZP)$$

constant, as  $N \Rightarrow B$ :

$$(BC/BC)(AC/AB)(ZB/ZC) \Rightarrow \mathbb{R}$$

38

Refraction through a circle's center occurs when N lies at B, so that an object's ray from A to N lies along ABC, and an image ray lies along BCZ. The locations of the object A and image Z along the optic axis BC are described by the equation:

$$\mathbb{R} = CO/CP = (AC/AB)(ZB/ZC)$$

39

If we draw A and Z along the optic axis BC as if it were a circle, and draw CDL so that  $AL \parallel ZB$ :  
 $\triangle ACB \cong \triangle ZCD$ , and:

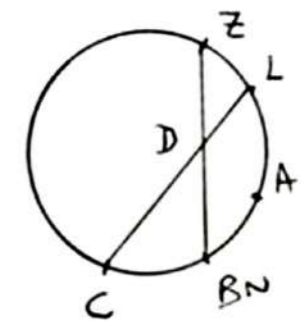
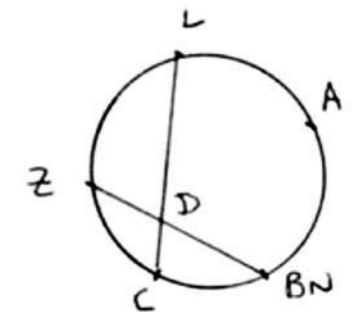
$$(AC/AB)(ZB/ZC) =$$

$$(ZC/ZD)(ZB/ZC) =$$

$$(ZB/ZD)$$

so as the reference circle's radius  $\Rightarrow \infty$ ,

$$(ZB/ZD) \Rightarrow \mathbb{R}$$



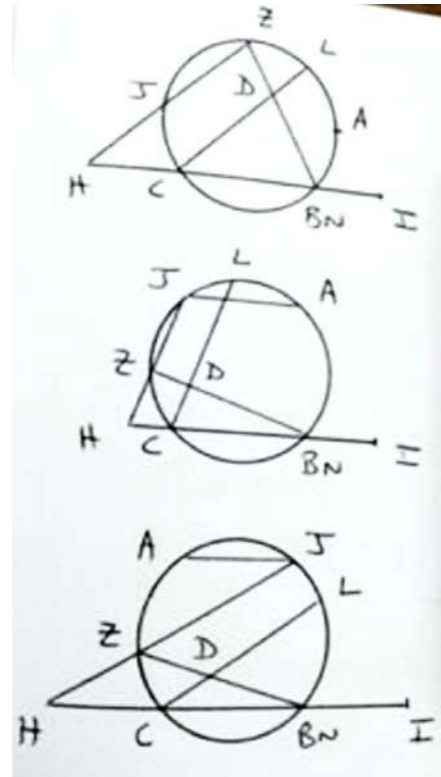
40

$$\begin{aligned} AL &\parallel ZB \\ AZ &= BL \\ \sim AZ &= \sim BL \end{aligned}$$

$$\begin{aligned} HZ &\parallel CL \\ ZC &= LJ \\ \sim ZC &= \sim LJ \end{aligned}$$

$$\begin{aligned} \sim AZ + \sim ZC &= \sim AZC \\ \sim BL + \sim LJ &= \sim BLJ \end{aligned}$$

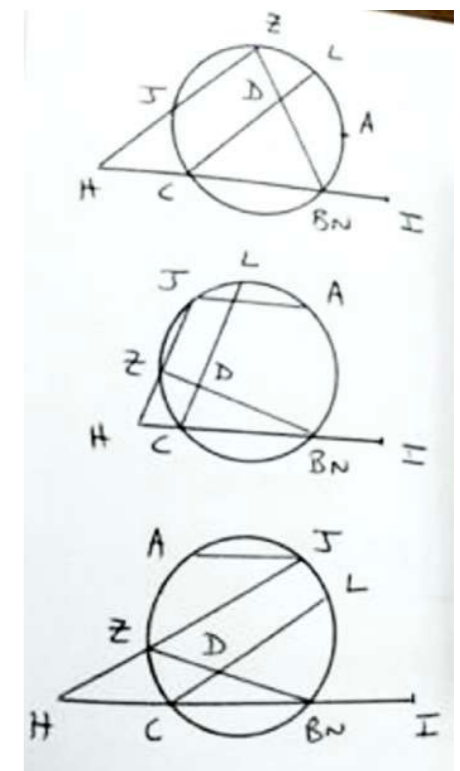
$$\begin{aligned} \sim AZC &= \sim BLJ \\ AJ &\parallel CB \end{aligned}$$



41

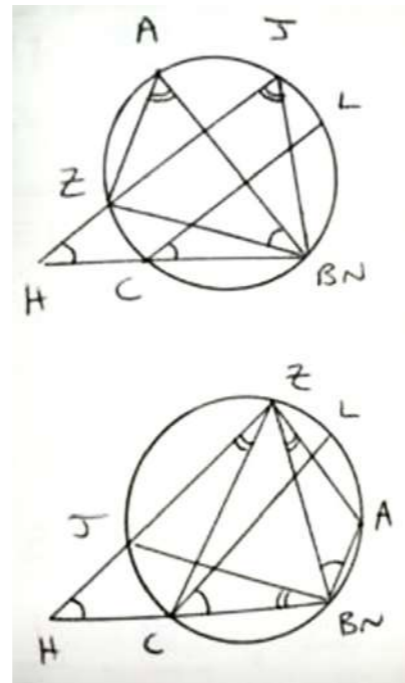
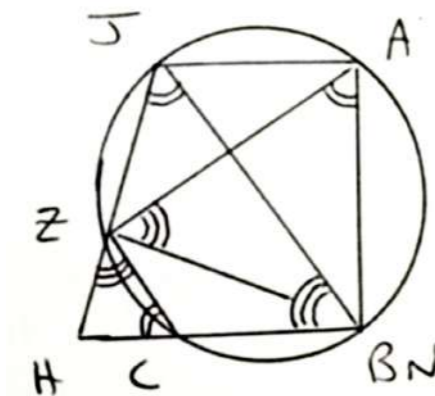
$$\begin{aligned} HZ &\parallel CL \\ ZB/ZD &= HB/HC \\ \Delta HBZ &\cong \Delta HJC \\ \text{when } \Delta HJC &= \Delta IAB: \\ HC &= IB, \text{ and:} \\ IB/IA &= HZ/HB \end{aligned}$$

This results in  
Newton's Equation:  
as the reference circle  
radius  $\Rightarrow \infty$ ,  
 $(AI)(ZH) = (BI)(BH)$



42

$$\begin{aligned} \Delta HCZ &\cong \Delta HJB \cong \Delta BAZ \\ (HC/HZ) &= (BA/BZ) \\ [1/(HZ)(BA)] &= [1/(HC)(BZ)] \end{aligned}$$



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as the reference circle's radius  $\Rightarrow \infty$ ,  
 $[1/(HZ)(BA)] = [1/(HC)(BZ)] \Rightarrow R/(HB)(BZ)$   
and the resulting possible sums occur:

$$\begin{aligned} HZ &= HB + BZ \\ HB &= HZ + BZ \\ BZ &= HZ + HB \end{aligned}$$

which, when multiplied by the above three  
factors, form the conjugate foci equations.

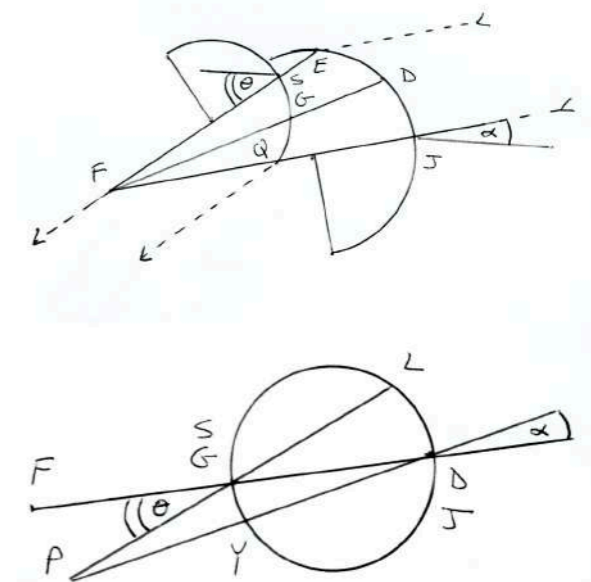
44

The conjugate foci equations allow for the effect of axial refraction at a circle to be expressed as the term:

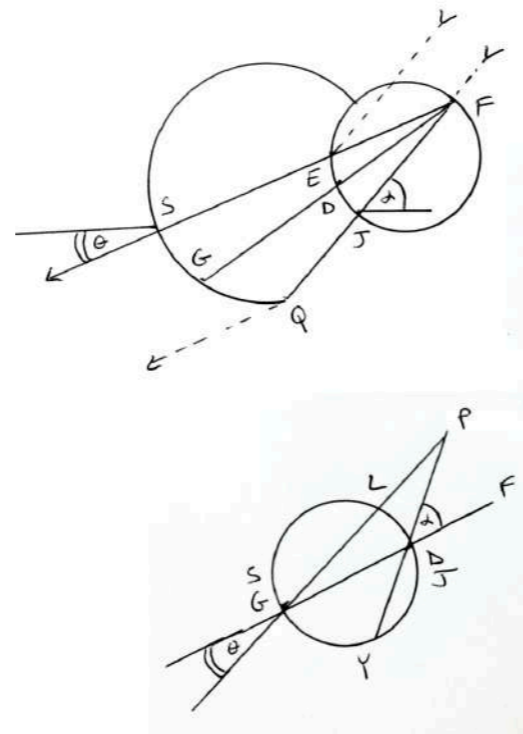
$$(1/HC) = (R/HB)$$

which is then additive with object vergence, defined as  $(1/BA)$ ; or image vergence, defined as  $(R/BZ)$ .

When distance refraction at  $\sim JDE$  is followed by refraction into distance at  $\sim QGS$  along axis  $DGF$  as shown; as  $\angle JFD = \angle SFG$ , and both approach zero:



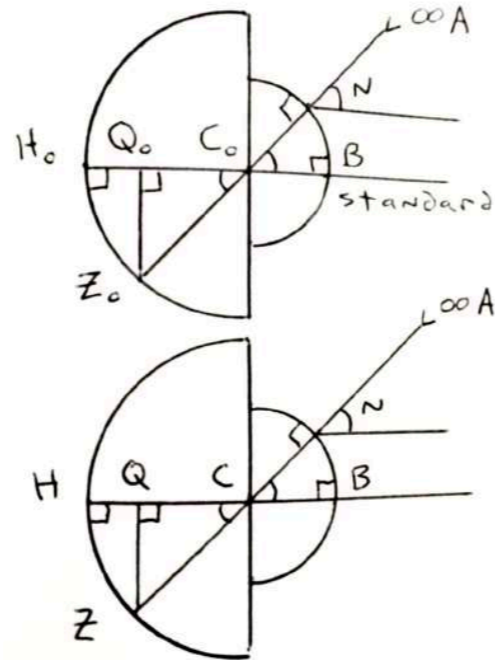
Or when distance refraction at  $\sim JDE$  is followed by refraction into distance at  $\sim QGS$  along axis  $FDG$ , as shown; as  $\angle JFD = \angle SFG$ , and both approach zero:



$\theta/\alpha \Rightarrow (\sim LD/GD)/(\sim YG/GD)$  as  $P \Rightarrow F$   
 $\theta/\alpha \Rightarrow (FD/FG)$  as  $P \Rightarrow F$   
 so that afocal axial angular magnification/minification equals:

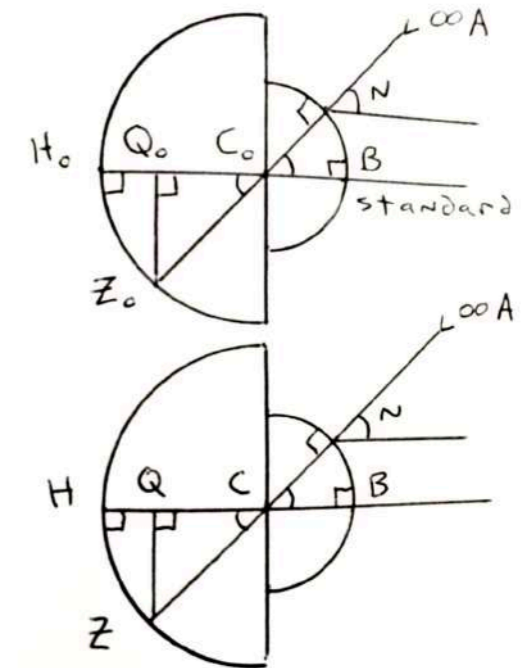
$$FD/FG$$

The top diagram illustrates a standard single-surfaced eye with a distant object A, and resulting retinal image size  $H_oZ_o$ .



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The bottom diagram illustrates any single-surfaced eye with a distant object A, and resulting retinal image size HZ.



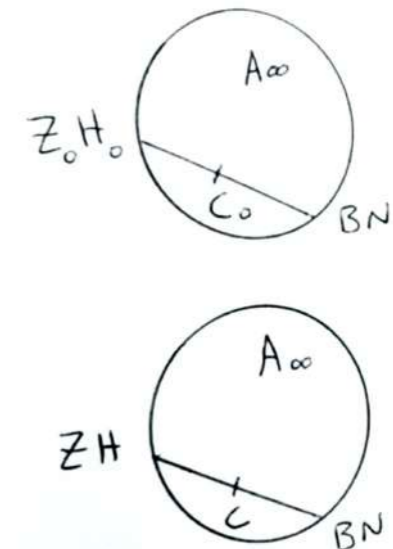
50

As  $N \Rightarrow B$ , the retinal image size magnification,  $ZH/Z_oH_o$ , (relative to an arbitrary standard which factors out with subsequent comparisons), then approaches its axial value:

$$\begin{aligned} ZQ/Z_oQ_o &= ZC/Z_oC_o = HC/H_oC_o \\ &= (BH/R)/(BH_o/R) = BH/BH_o \end{aligned}$$

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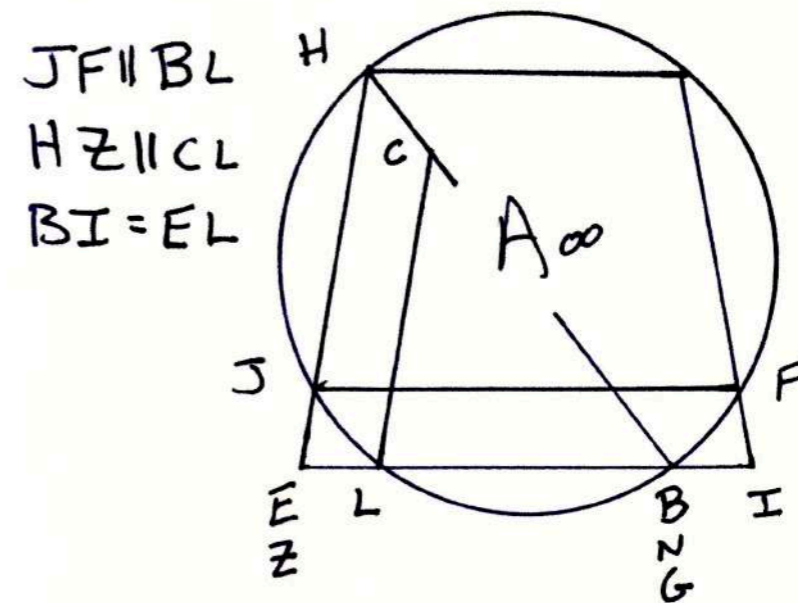
Once again representing the optic axis BCZ as a circle of infinite radius, the distant object A at  $\infty$  is focused by the radius BC of the presumed single refracting surface towards the axial image Z, which lies at the retina H when there is no distance refractive error. ( $BH_o$  represents the standard axial length, and  $BC_o$  represents the standard single refracting curvature radius).



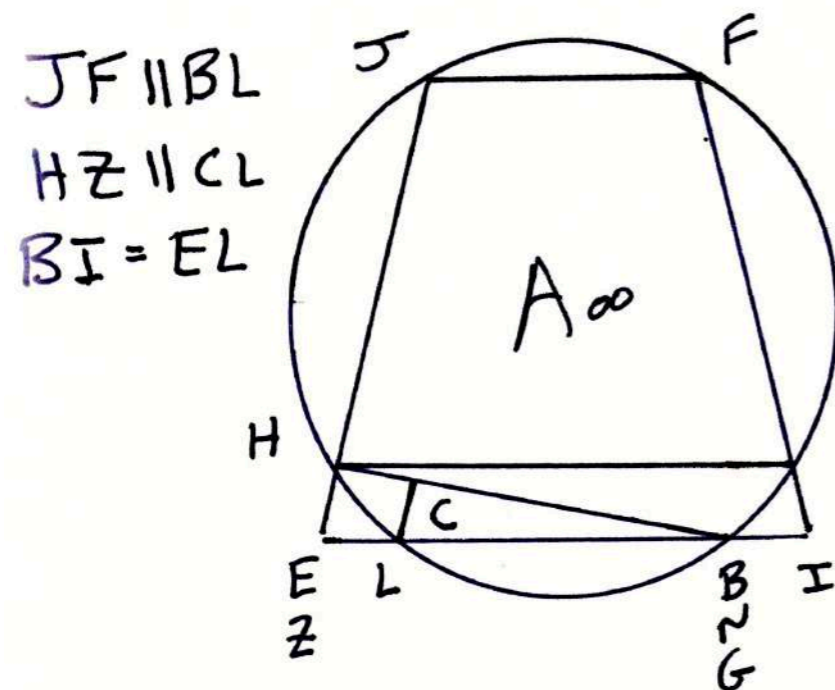
52

As pictured in the next three slides, additional refraction G (at B) will create an “ametropic” eye, with “distance refractive error,” and a combination curvature effect with total radius BL instead of BC, moving image Z from the retina at H to its erroneous location at E. The “front focal point” of the “ametropic” eye is defined as point I. A “distance correction” must focus the distant object towards F, so that  $JF \parallel BL$ , in order to move image Z back to the retina H.

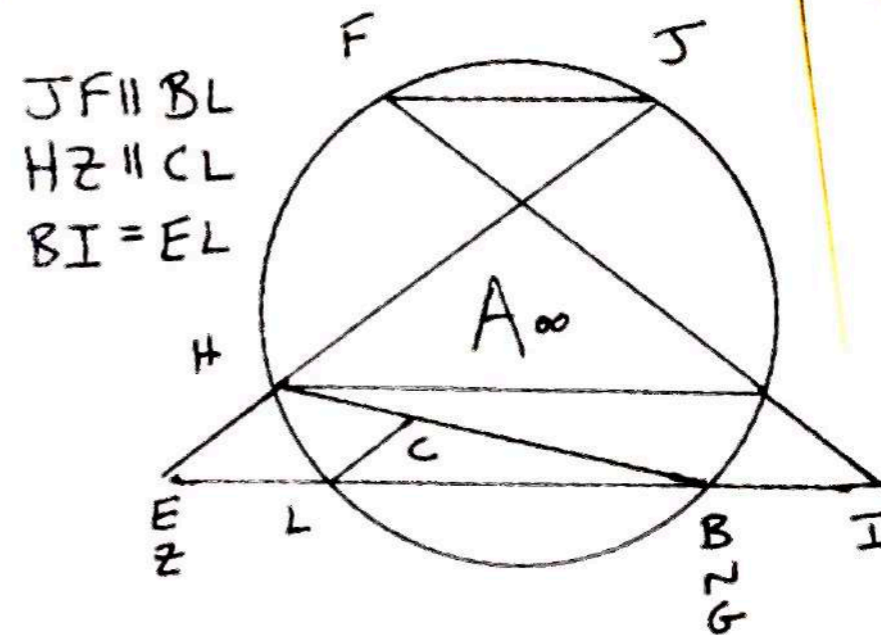
53



54

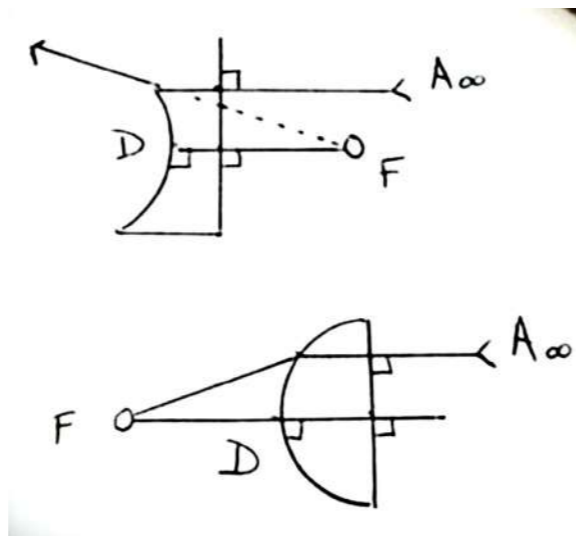


55



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The distance correction at D:



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Since the distance correction D moves image Z from E to retina H, rays leaving the refractive error G (at B) after this correction is in place must be afocal. This results in afocal axial angular magnification equaling:

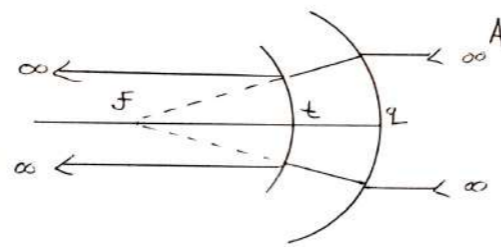
$$FD/FG (= FD/FB)$$

Therefore, the total axial magnification of distance correction equals:

$$M = (BH/BH_0)(FD/FB)$$

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When the front surface of a spectacle lens that corrects distance refractive error is not flat, it is convex; and adds an additional “shape” factor,  $(fq/ft)$ , to the afocal axial magnification of distance correction. (Point “t” lies at D, and  $FD/FB$  remains the “power” factor of the afocal axial magnification of distance correction).



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“Axial Ametropia” occurs when E is at  $H_0$ , (and point I is therefore at  $I_0$ , the front focal point of the standard eye). The distance refractive error is then completely due to an axial length BZ, (or BH), that is not standard.

$$\Delta H_0BH = \Delta EBH \cong \Delta E JL = \Delta I_0FB$$

$$(BH/BH_0) = (FB/FI_0)$$

$$M = (FB/FI_0)(FD/FB) = FD/FI_0$$

Therefore, in the case of axial ametropia, there is no total axial magnification of distance correction if the correction D lies at  $I_0$ .

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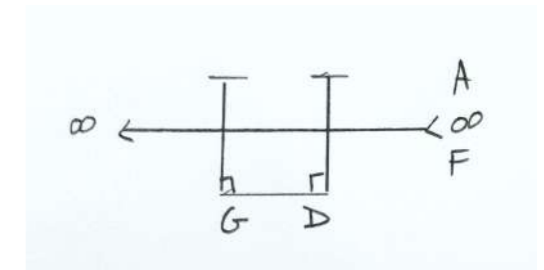
“Refractive Ametropia” occurs when the retina H is at at  $H_0$ . The distance refractive error at G moving image Z to E is then completely due to a refracting radius BL that is not the standard  $BC_0$ .

When the distance correction D lies at B:

$$M = (BH/BH_0)(FD/FB) = 1$$

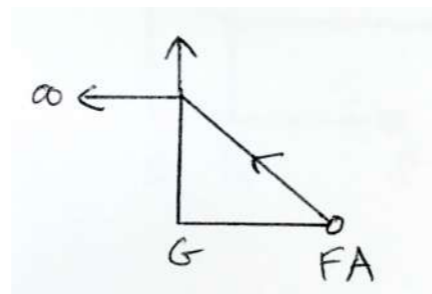
61

There is no afocal axial angular magnification of distance correction with a distant object “A,” and an emetropic eye whose refractive error at G (at B) is by definition zero, (with its focal point F at infinity).



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There is also no afocal axial angular magnification when object A is at the front focal point F of an uncorrected ametropic eye as shown, since this “myopic” system is not afocal, and involves only one refracting element G.

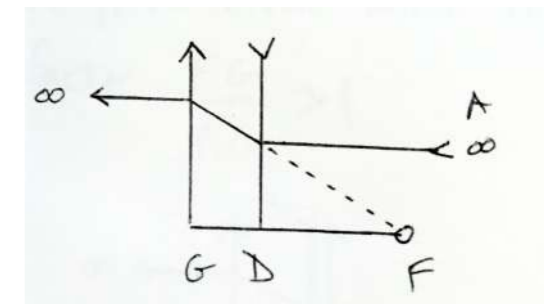


63

A distance myopic correction at D creates afocal axial angular minification:

$$FD/FG < 1$$

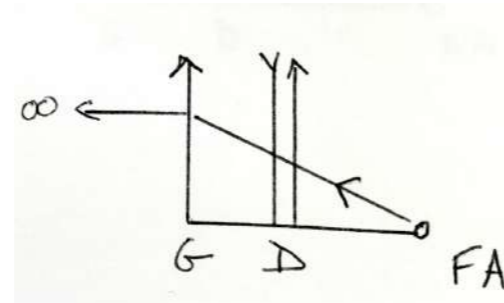
and this is relative to either the myopic eye with object A at its front focal point F, or the emetropic eye with object A at distance.



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Removing the myopic distance correction at D with a converging lens at G removes this afocal axial angular magnification with the factor:

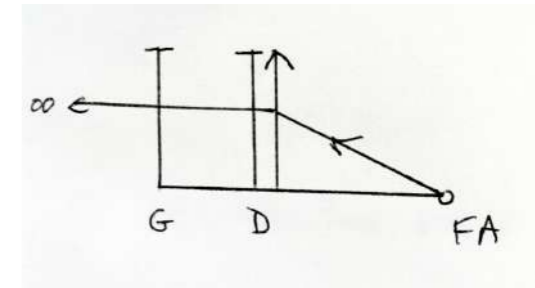


$$FG/FD > 1$$

and this magnification of near correction is relative to the distance corrected myope.

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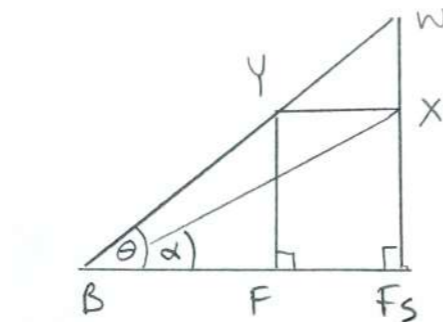
If additional converging power is added to the converging lens so that the near focal point is in focus for an emetropic eye, which we then consider to be the reference eye, the magnification of near correction is still that which is removed with the factor:



$$FG/FD > 1$$

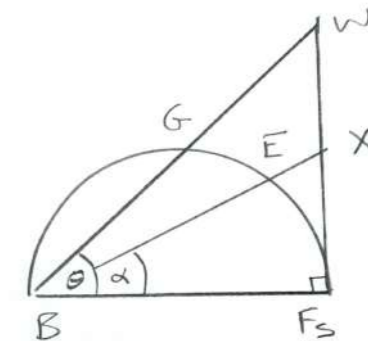
66

When an object at a standard distance  $F_s$  is moved to F:



67

The object angular subtense magnification equals:



$$\theta/\alpha = (\sim GF_s/BF_s)/(\sim EF_s/BF_s)$$

68

as  $XFs \Rightarrow 0$

the object angular subtense magnification approaches its axial value:

$$\theta/\alpha \Rightarrow WFs/XFs = WFs/YF = BFs/BF$$

which equals the axial object angular subtense magnification.

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The ratio describing axial object angular subtense magnification:

$$BFs/BF$$

when multiplied by the ratio describing near magnification due to a single converging lens producing parallel light for an emmetropic eye:

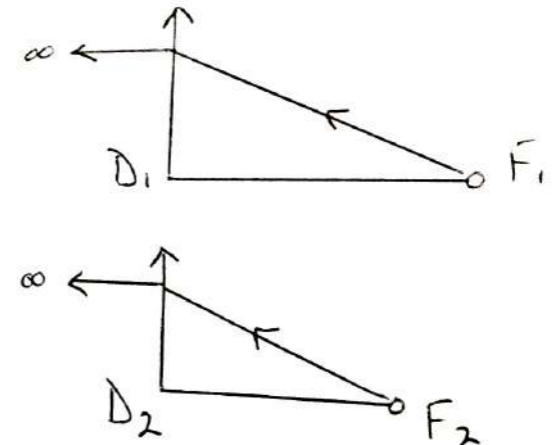
$$FB/FD$$

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produces a ratio which factors out the object's actual distance to the eye, confirming that when a converging lens is used with its front focal point at the object, so that parallel light leaves the converging lens from the object, the image size is the same regardless of the object-to-eye distance.

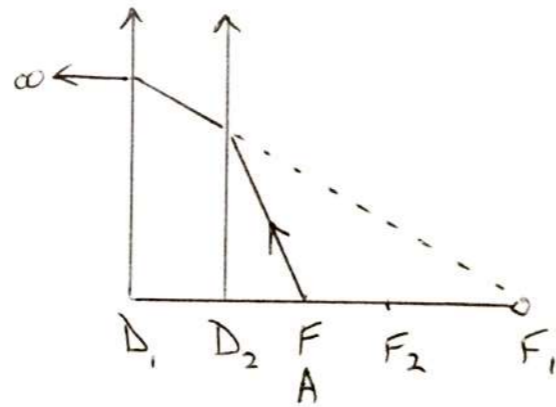
71

When the converging lens at D is split into two converging lenses:



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with the same  
combined  
focus F:



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the ratio describing axial near magnification  
due to a single converging lens producing  
parallel light for an emmetropic eye:

$$FB/FD$$

must be expressed *as if* all convergence  
occurred at a single unknown axial point De:

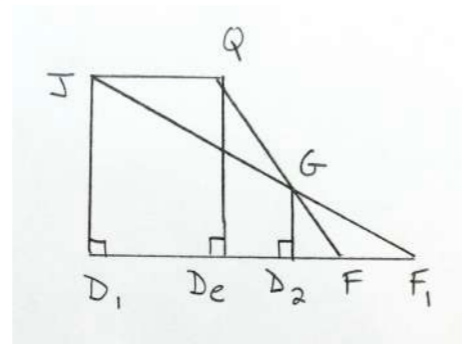
$$FB/FDe$$

74

De can be located using  
triangles.

$$D_2G/D_2F = DeQ/DeF$$

$$D_2G/D_2F_1 = D_1J/D_1F_1$$



$$D_2F(DeQ/DeF) = D_2F_1(D_1J/D_1F_1)$$

$$DeQ/DeF = (D_2F_1/D_2F)(D_1J/D_1F_1)$$

$$1/DeF = (D_2F_1/D_2F)(1/D_1F_1)$$

$$FB/FDe = (D_2F_1/D_2F)(FB/D_1F_1)$$

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Multiplying the axial object subtense  
magnification by the axial  
magnification of near correction  
(relative to the same eye without  
refractive error) produces:

$$BFs/FDe = (D_2F_1/D_2F)(BFs/D_1F_1)$$

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The converging lens  $D_2$  creates a virtual image  $F_1$  of an object at  $F$ . When considering a stand magnifier with lens  $D_2$ , constant stand height  $D_2F$ , and reading spectacle add or ocular accommodation  $D_1$ , the stand magnifier's (constant) enlargement of the object at  $F$  equals:

$$E = D_2F_1/D_2F$$

The stand magnifier's axial magnification is its (constant) enlargement factor  $E$ , multiplied by what would be produced by  $D_1$  alone, if the object  $A$  were at  $F_1$ .