

Axial Magnification

Plane Geometry Approach

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2021

Dedicated to my Geometrical Optics professor, William Brown, OD, PhD, who always taught the geometry first.

Reference:

Isaac Barrows Optical Lectures, 1667

Translated by H.C. Fay

Edited by A.G. Bennett

Publisher:

The Worshipful Company of Spectacle Makers

London, England; 1987

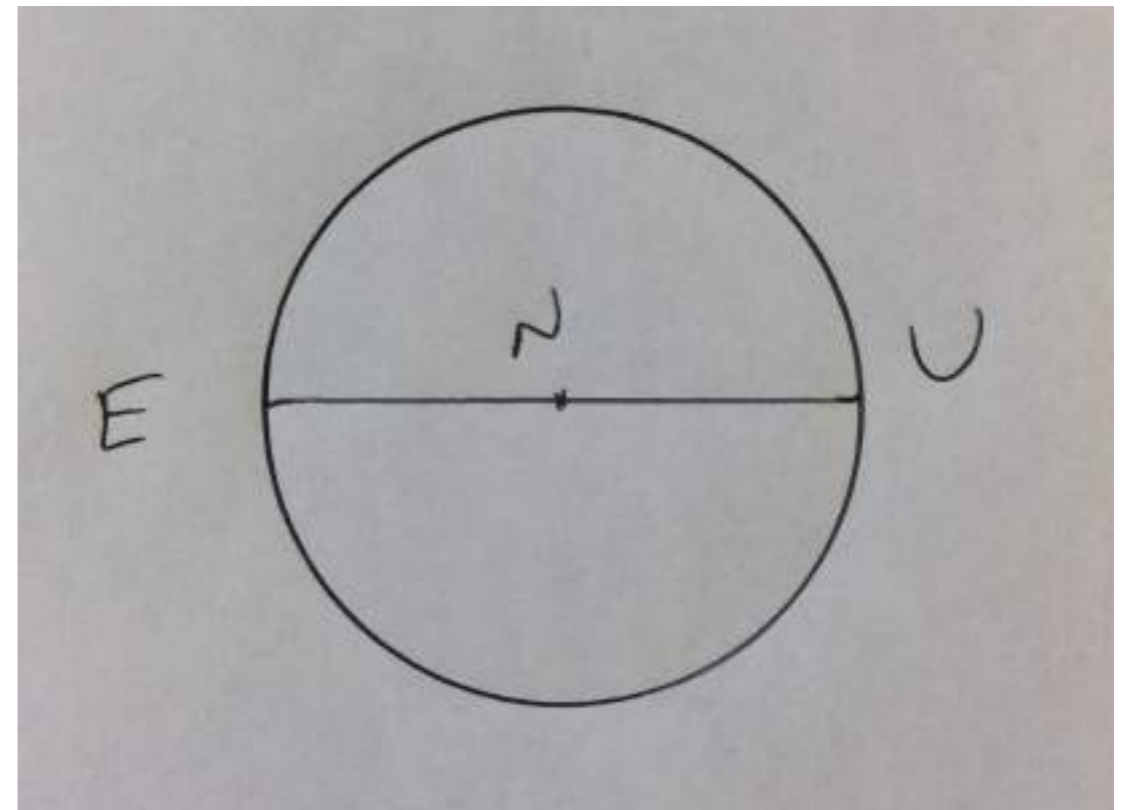
ISBN # 0-951-2217-0-1

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1). prerequisite geometry

On a circle with diameter EU and center N:



Two equal arcs $\sim SE$ and $\sim JR$ can be shown to subtend equal angles by drawing any two parallel lines SD and JF . Since parallel lines intercept equal arcs across a circle,

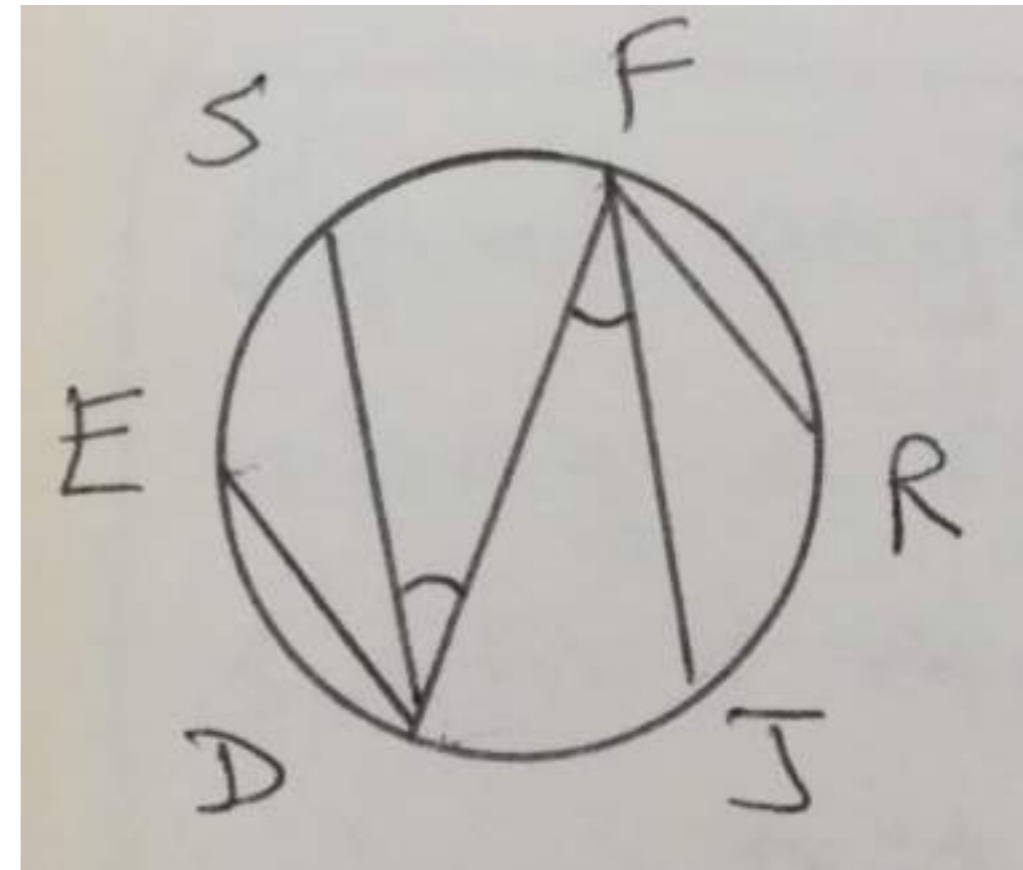
$$\sim SF = \sim JD$$

$$\sim SE + \sim SF = \sim JR + \sim JD$$

$$\sim EF = \sim RD$$

$ED \parallel RF$, and therefore:

$$\angle SDE = \angle JFR$$



Since conversely, equal angles along a circle subtend equal arcs, any angle along any circle can be defined in terms of its subtended arc and the circle's diameter.

For example: $\angle RFJ = \sim RJ/EU$

$$\angle KNU = \angle MDH$$

$$\angle MDH = \sim MH/MD$$

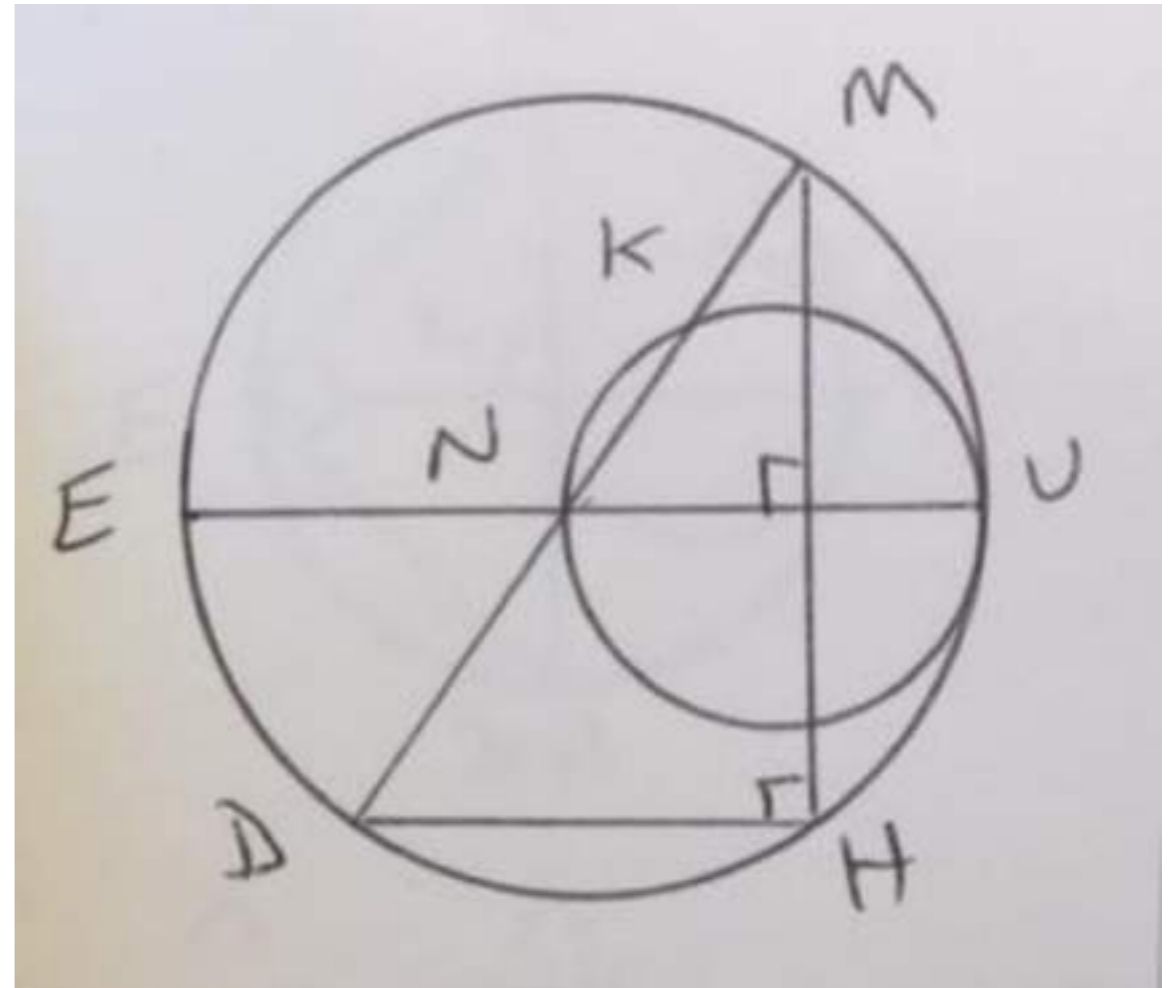
$$= \sim MH/UE = 2(\sim UM)/UE$$

$$= 2\angle MEU$$

$$\angle KNU = \sim UK/UN$$

$$= 2(\sim UM)/2(UN)$$

$$\sim UK = \sim UM$$

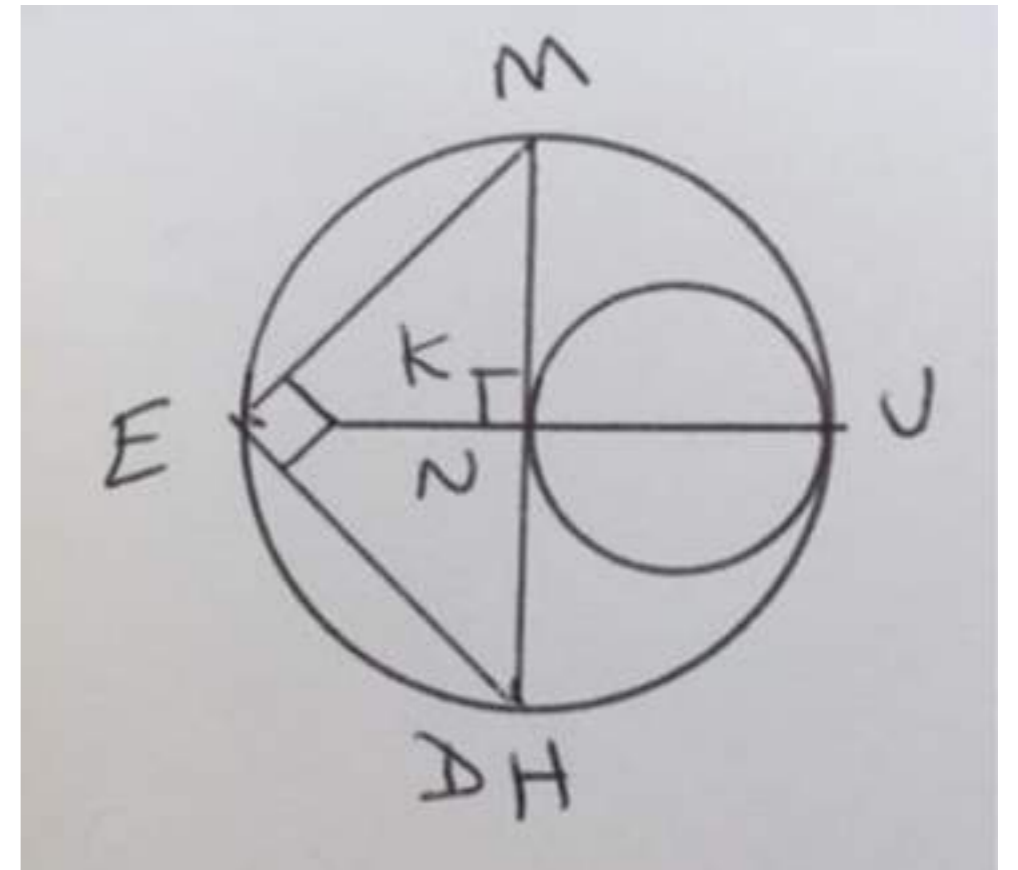


Let $K \Rightarrow N$ and $D \Rightarrow H$:

$$\begin{aligned} \sim UK/UN &= \sim MH/MD \\ &= \sim MH/UE = \angle MEH \end{aligned}$$

$$\sim UK/UN = \angle MNU$$

$$2(\sim UK)/UN = \angle MNH = \pi$$



$$NS/NC = NC/NB$$

$$NK/NC = CN/CK$$

$$\triangle NSC = \triangle KWB = \triangle KNP$$

$$NC = KP$$

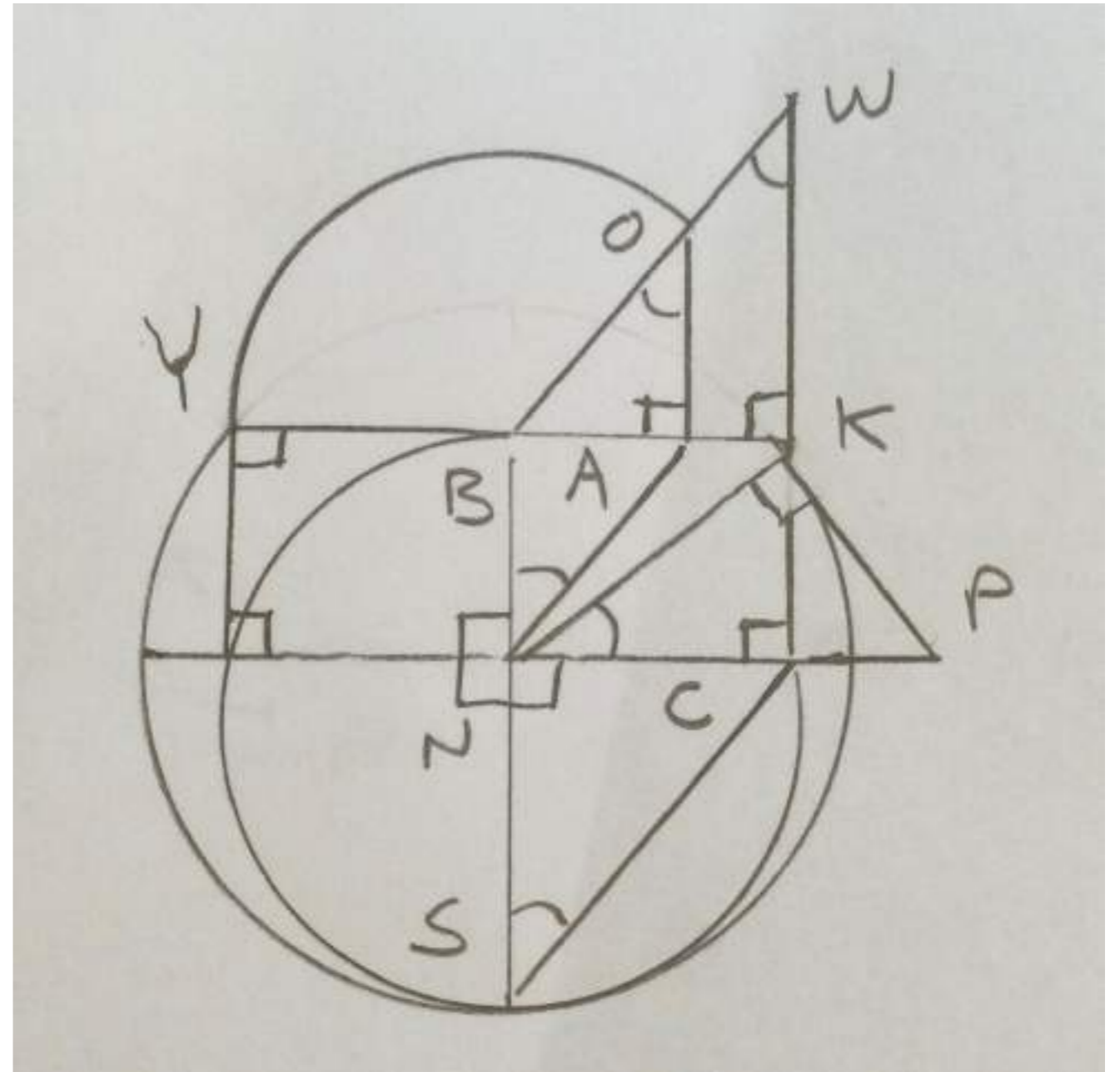
$$\triangle CKP = \triangle BNA = \triangle AOB$$

$$NA = KP$$

$$NC = NA = OB$$

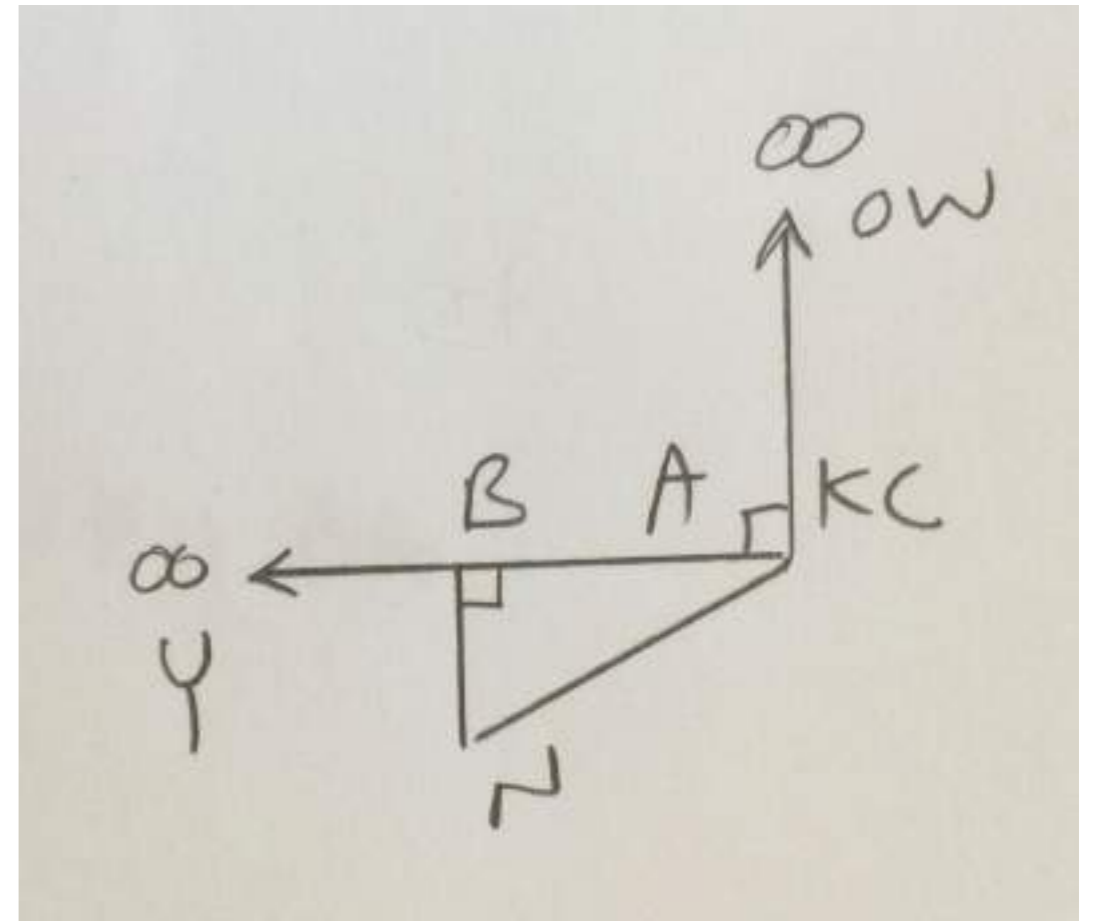
$$NC = KB = YB$$

$$\mathbf{WK = NS = YN}$$



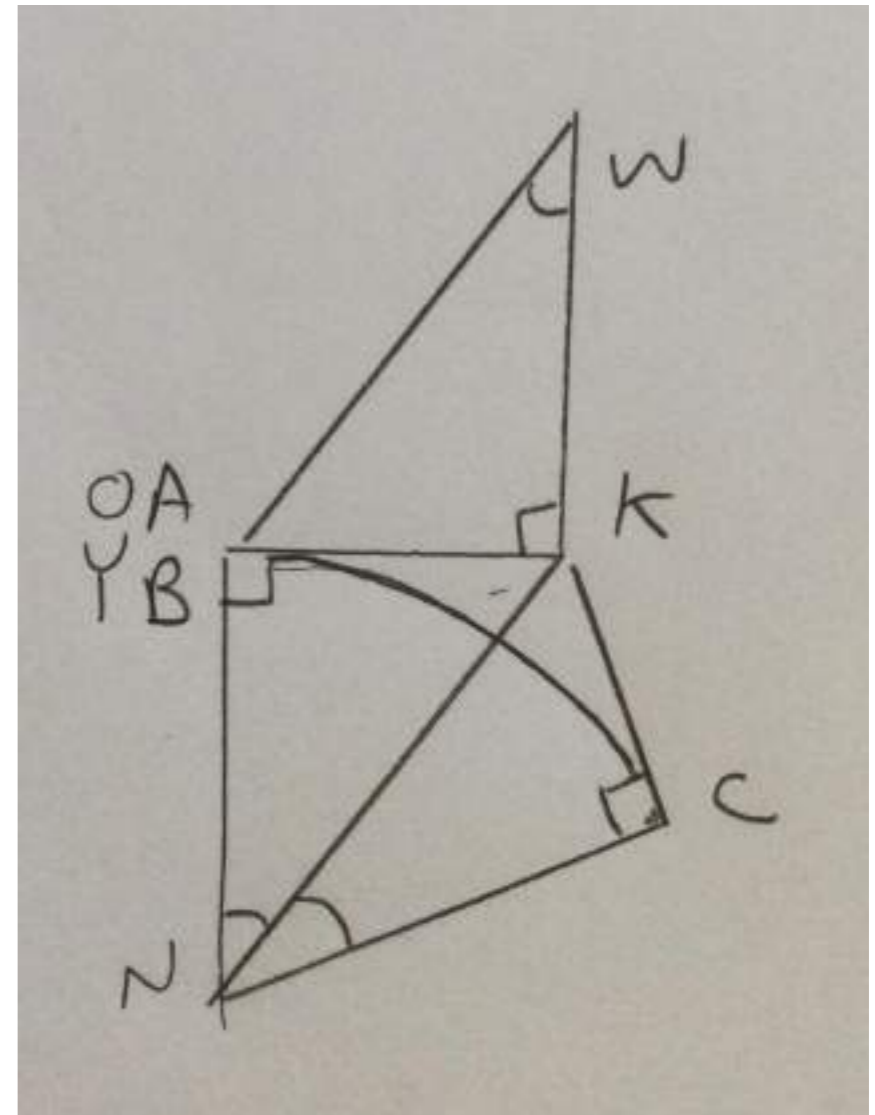
Keeping only:
 $NA = NC$, and
 $\triangle CNK \cong \triangle AOB \cong \triangle KWB$:

As $A \Rightarrow K$, $WK \Rightarrow YN$



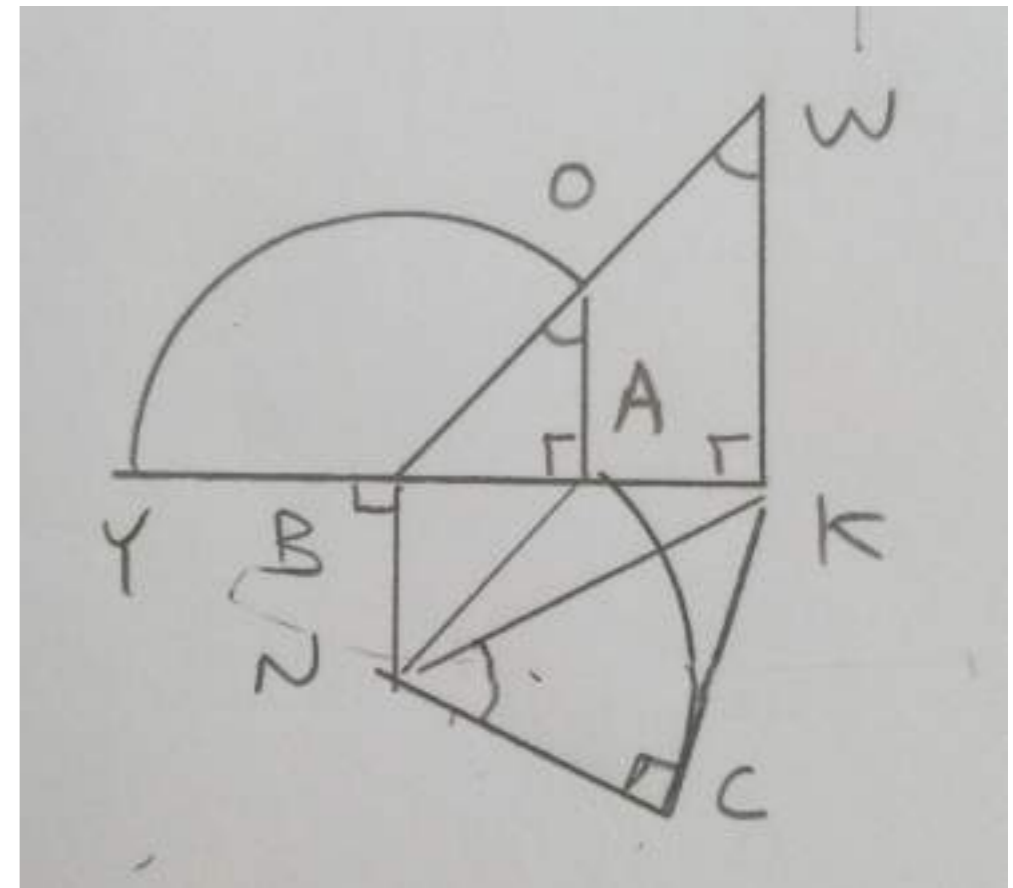
Keeping only:
 $NA = NC$, and
 $\triangle CNK \cong \triangle AOB \cong \triangle KWB$:

As $A \Rightarrow B$, $WK \Rightarrow YN$



We can therefore assume that whenever A lies on BK , given right triangle KBN , if $NA = NC$, and $\triangle CNK \cong \triangle AOB \cong \triangle KWB$ as shown, then:

$$WK = YN$$



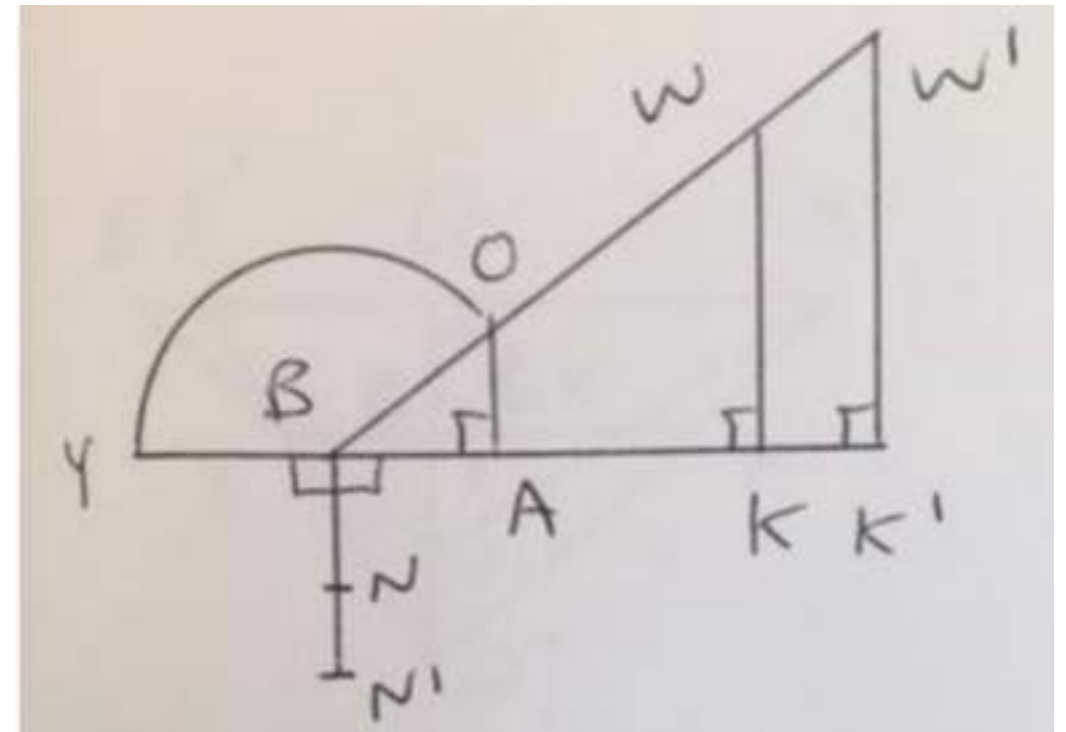
$$OB/OA = NK/NA$$

$$= N'K'/N'A$$

$$KW = YN$$

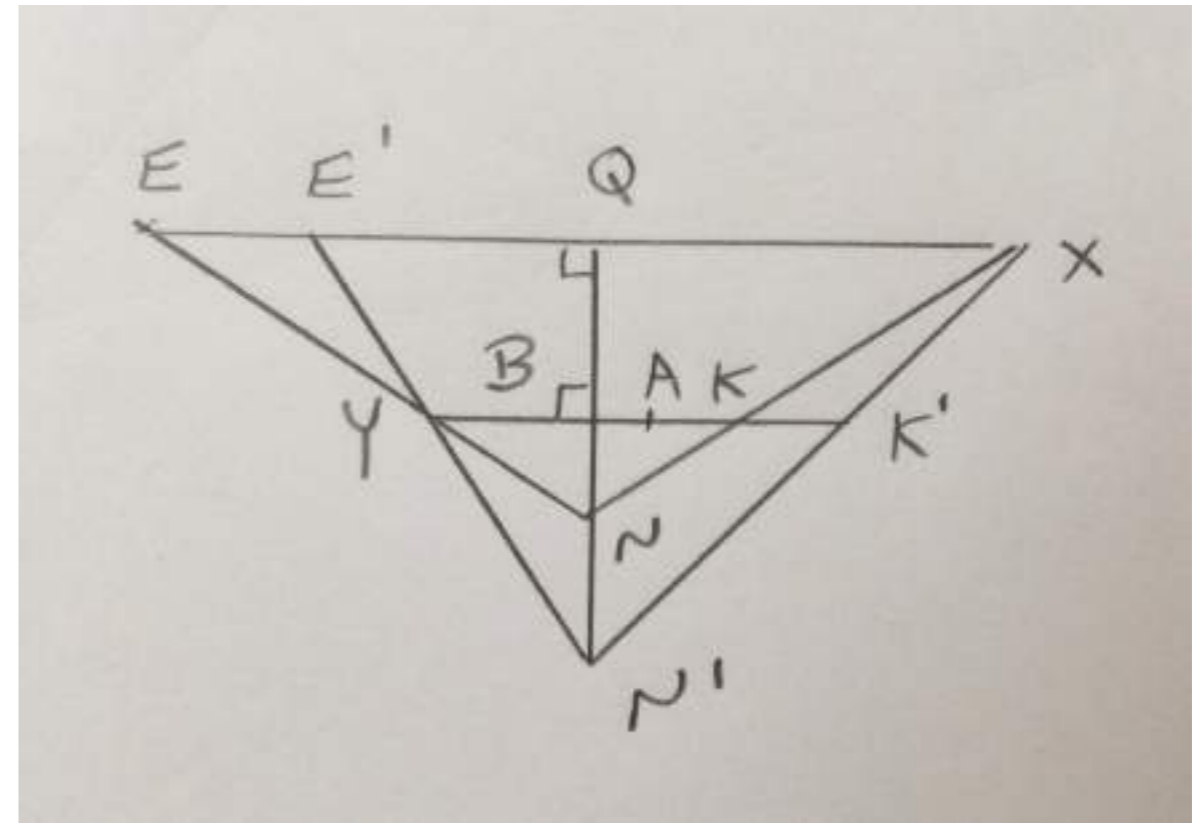
$$K'W' = YN'$$

$$KB/YN = K'B/YN'$$



$$\begin{aligned}
 QX/EN &= KB/YN \\
 &= K'B/YN' = QX/E'N'
 \end{aligned}$$

$$EN = E'N'$$

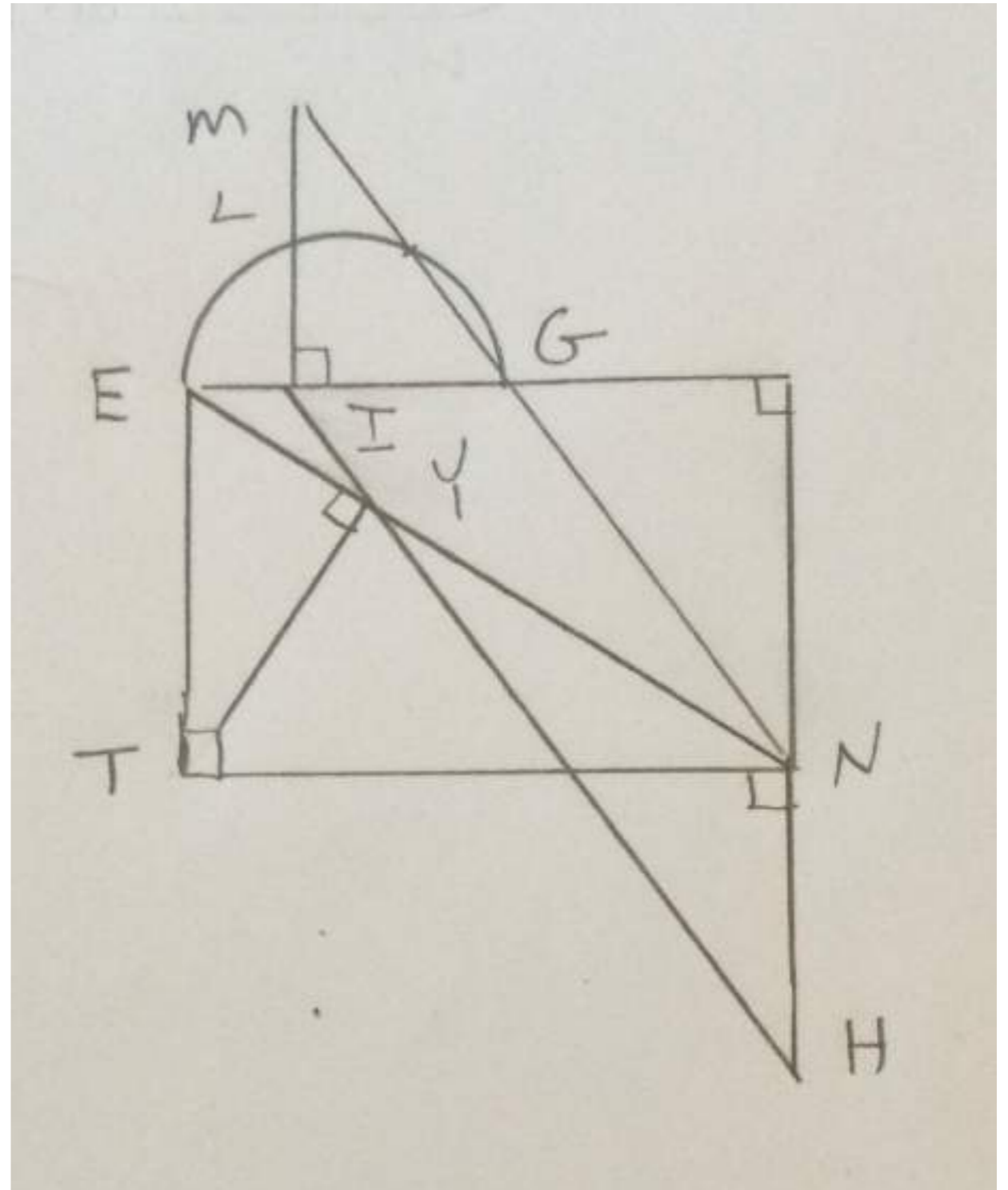


Only one $N'K'X$ exists for NKX since only one $E'N'$ exists equal to EN . When EN is the smallest segment through Y included in the right angle EQN , E' lies at E , and N' lies at N .

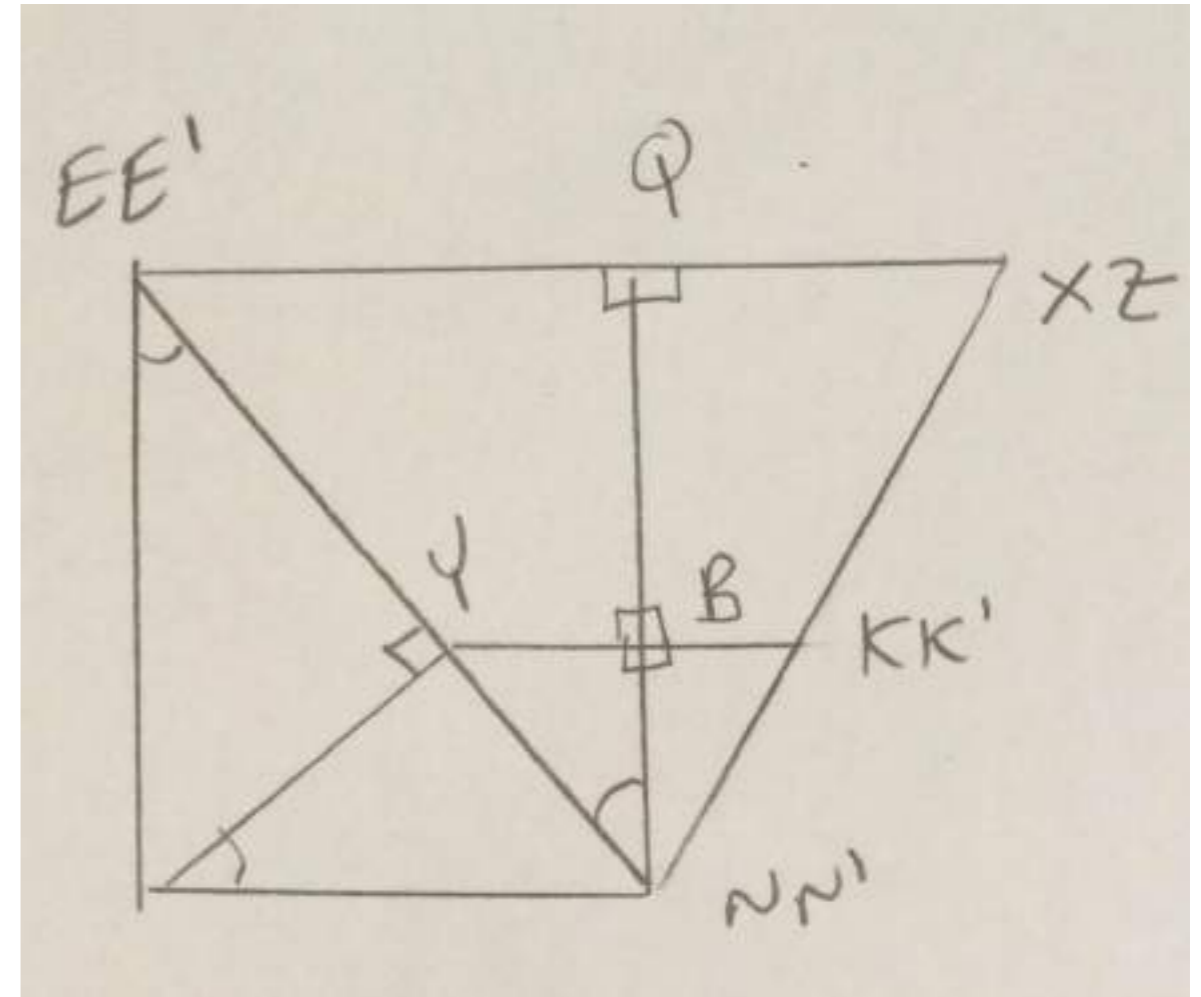
$NE \parallel GL$
 $TY \parallel EL$
 $HI \parallel NM$
 $HI = NM$
 $NM > NL$

NL is the hypotenuse
of right triangle NEL

$NL > NE$
 $HI > NE$

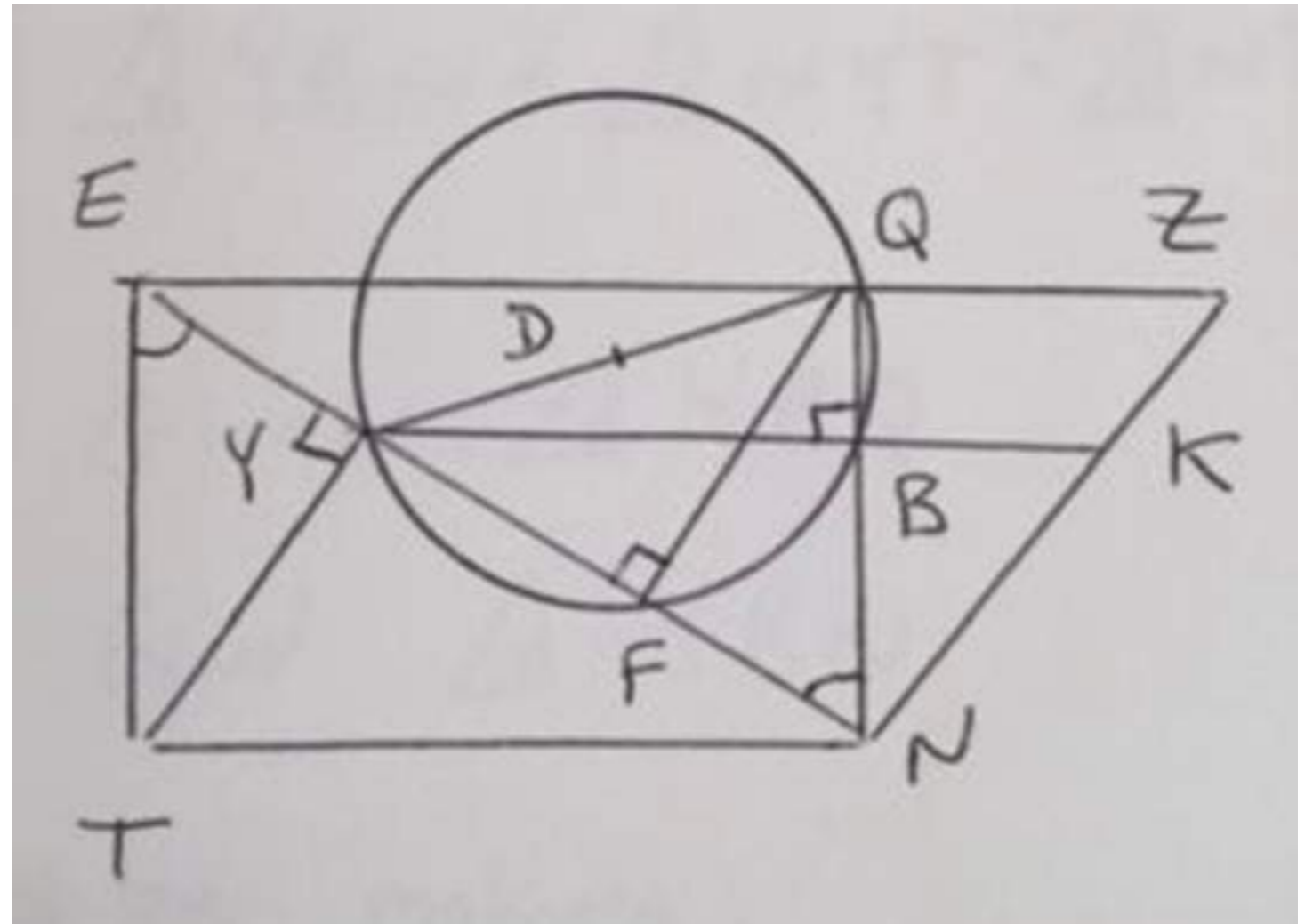


$X = Z$ when EN is the shortest segment through Y included in right angle EQN



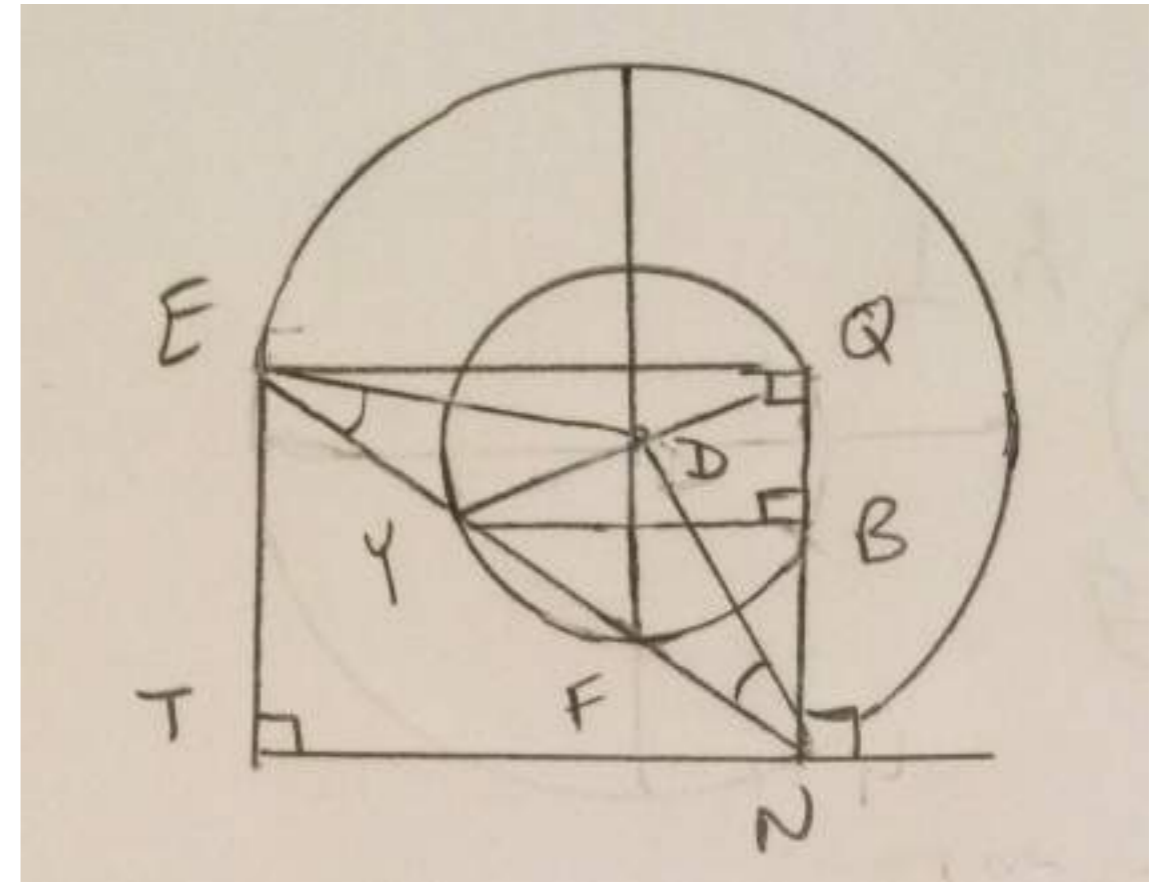
In order to find Z given $\triangle YBN$ and NK, we must find E using:

$$\begin{aligned} \triangle YBN & \\ &\cong \triangle NYT \\ &\cong \triangle NTE \end{aligned}$$



Not only does:
 $DY = DF$, but also:
 $ED = ND$ and therefore
 $\triangle EDY = \triangle NDF$
 so $EY = NF$

Since $\triangle QFN$ is a right triangle, so is $\triangle TYE$.
 Once we have found EN , we must also find NK in order to find Z .



2). refraction along a line

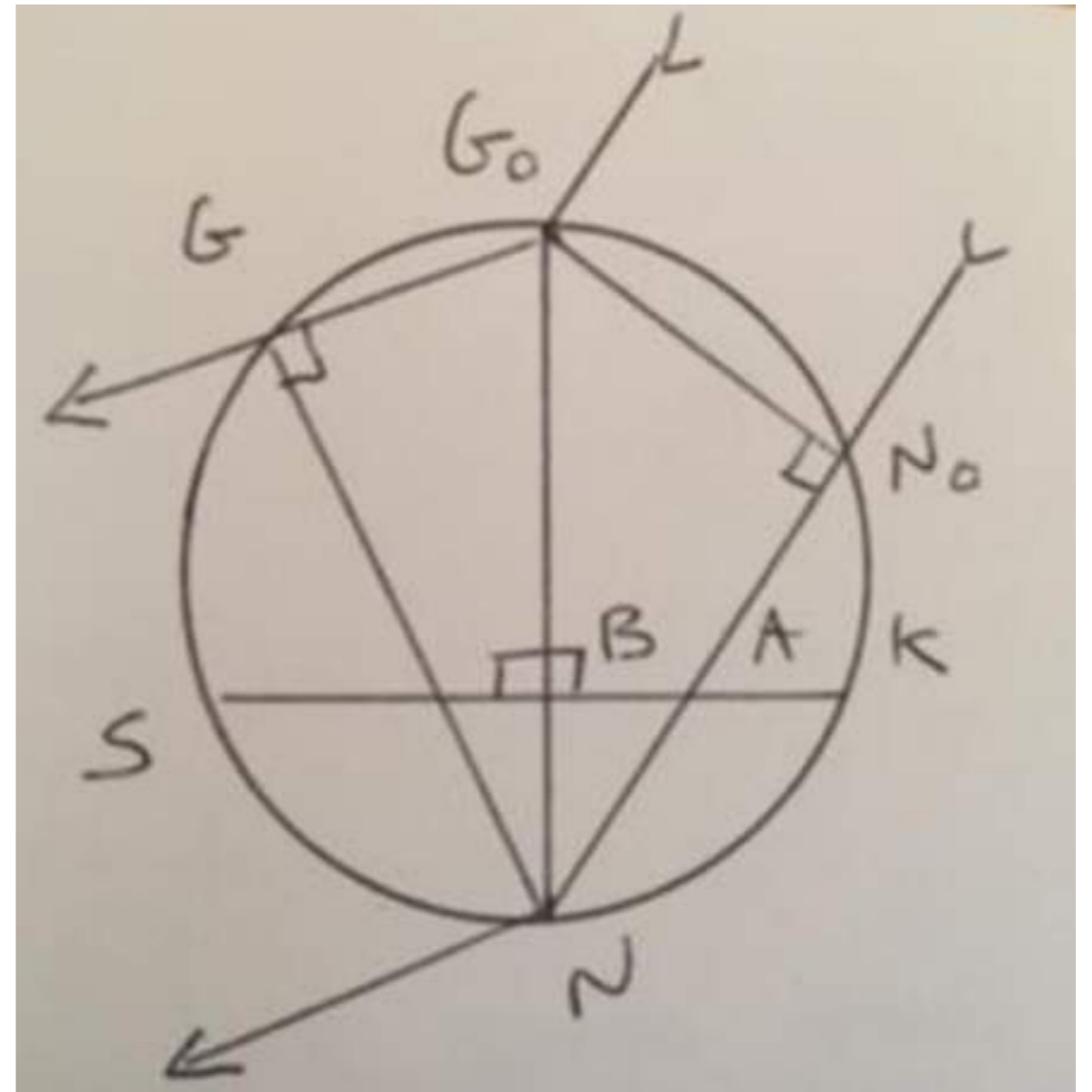
$$\Delta N_0NK \cong \Delta KNA$$

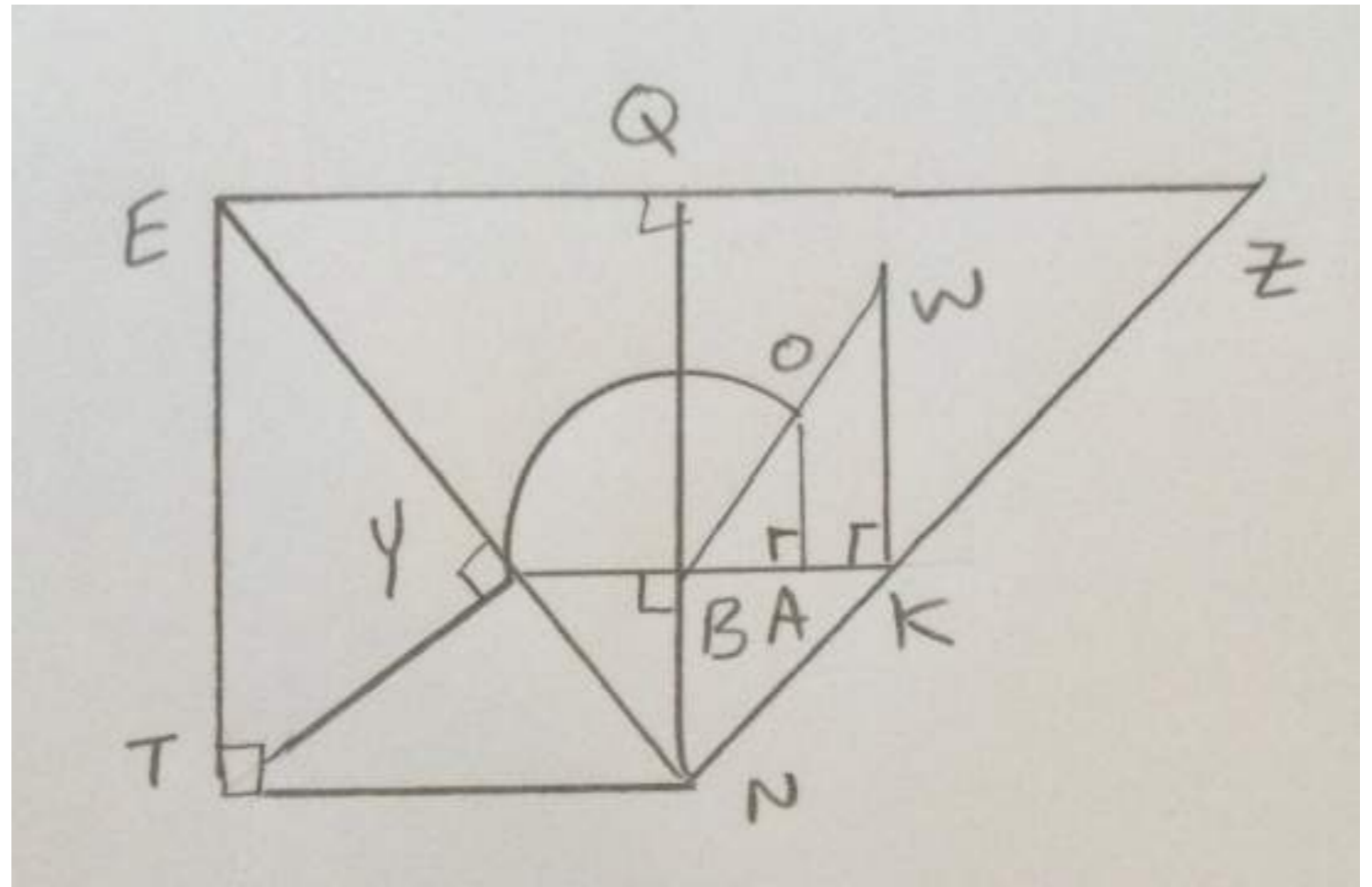
because:

$$\sim NS = \sim NK$$

Wavefront G_0N_0 refracts into wavefront GN along G_0N , because it travels G_0G in the same time it travels N_0N .

$$\begin{aligned} R &= NN_0/GG_0 \\ &= NN_0/NK = NK/NA \end{aligned}$$





given $\triangle BAO$:

use $\triangle BKW$ or $\triangle QBY$ to find $\triangle BNY$

use $\triangle BNY$ to find $\triangle BKW$ or $\triangle QBY$

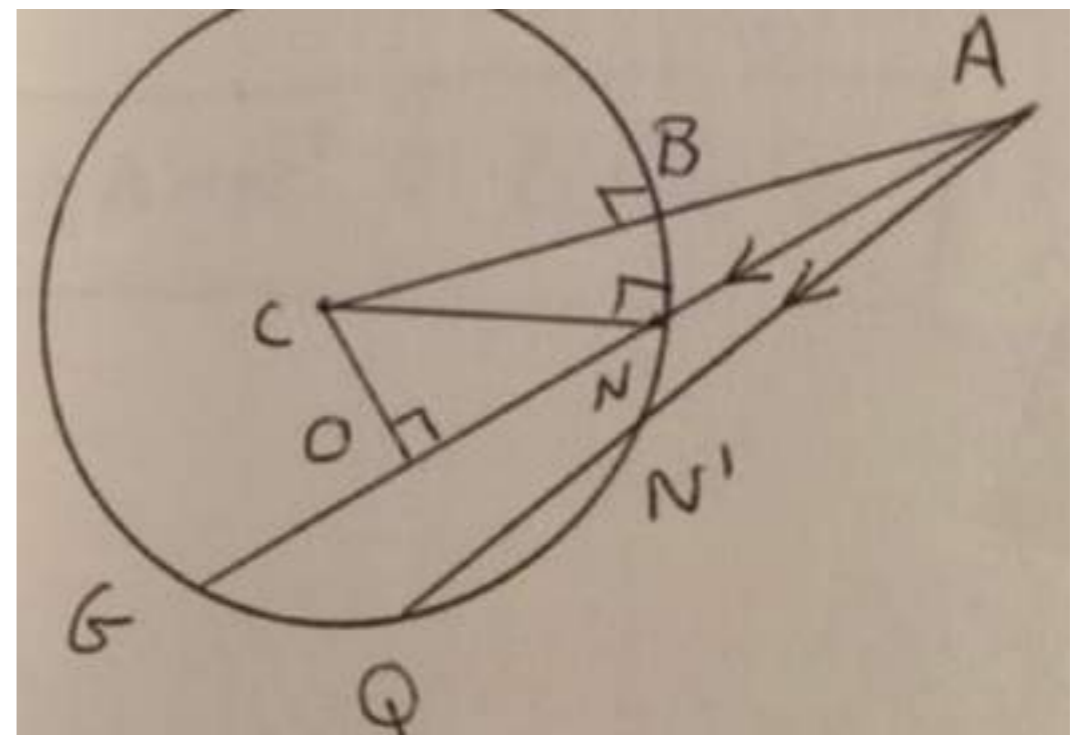
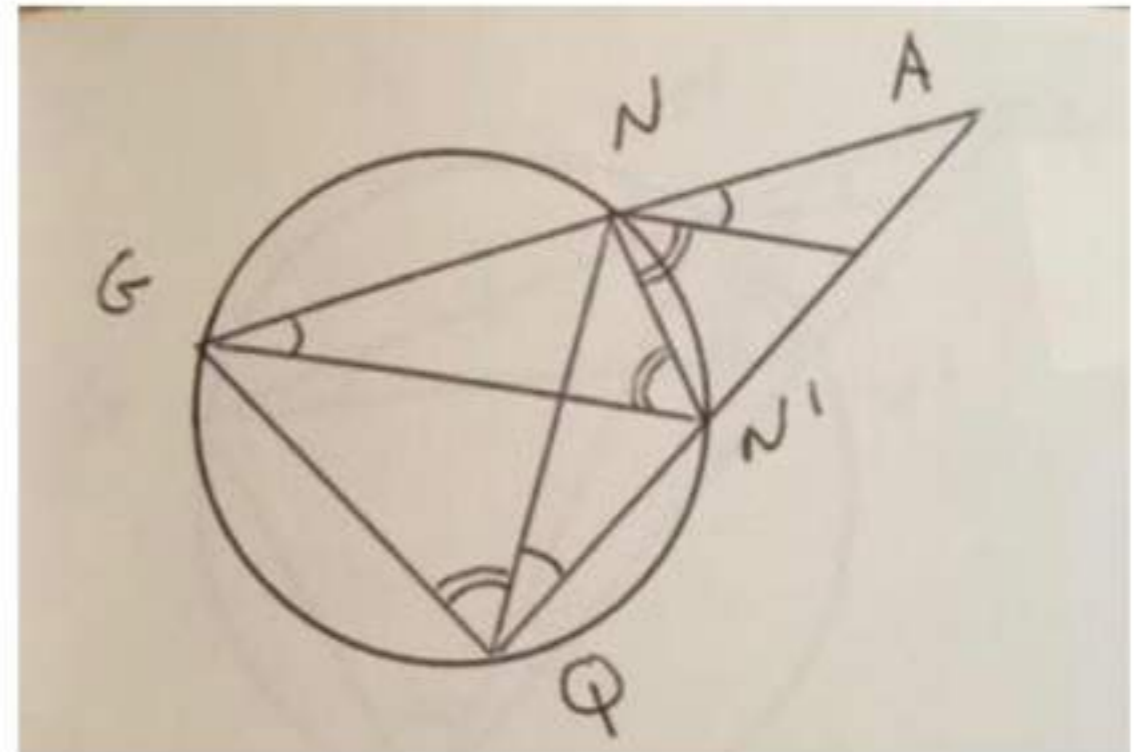
3). refraction along a circle

$$\Delta ANN' \cong \Delta AQQ$$

$$AG/AN' = QG/NN'$$

$$\begin{aligned} & (AG + AN')/2AN' \\ &= (QG + NN')/2NN' \end{aligned}$$

Real object A

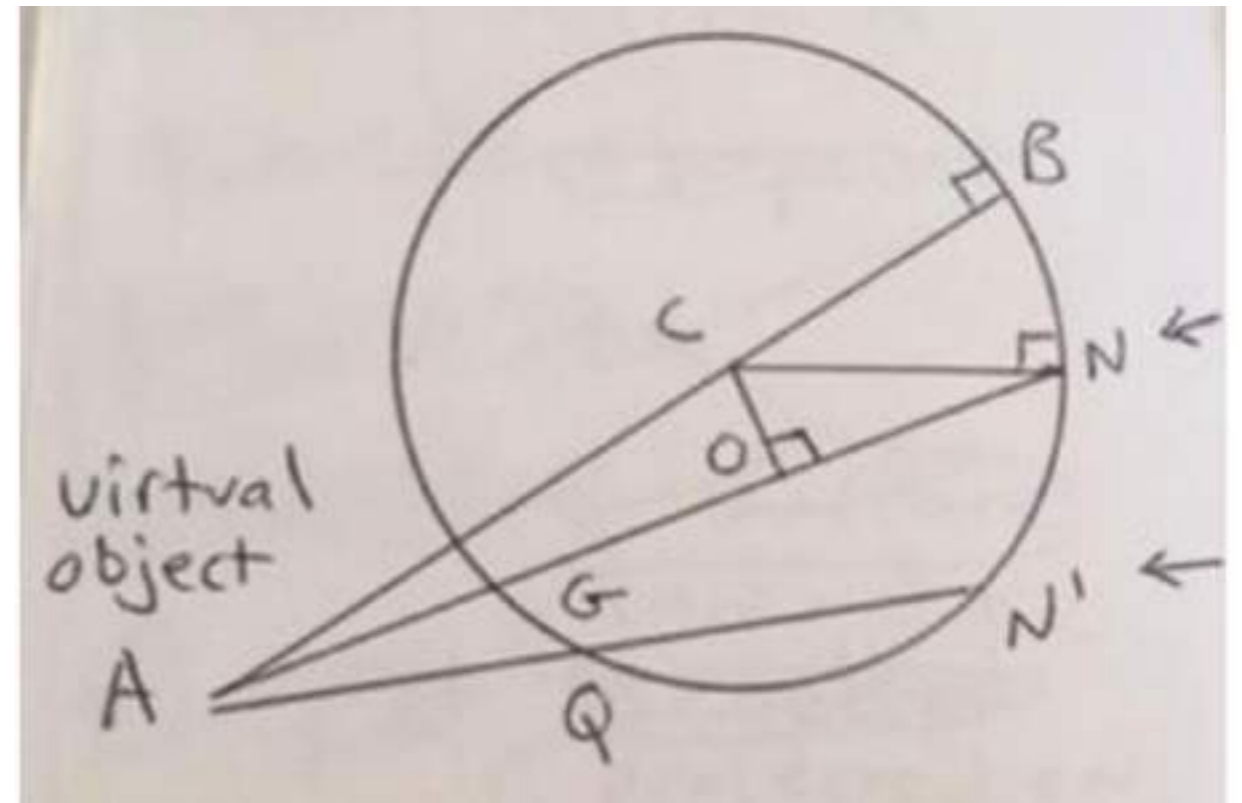


$$\Delta ANN' \cong \Delta AQQ$$

$$AG/AN' = QG/NN'$$

$$\begin{aligned} (AG + AN')/2AN' \\ = (QG + NN')/2NN' \end{aligned}$$

Virtual object A
can not be projected
on a screen due to
refraction at BN.

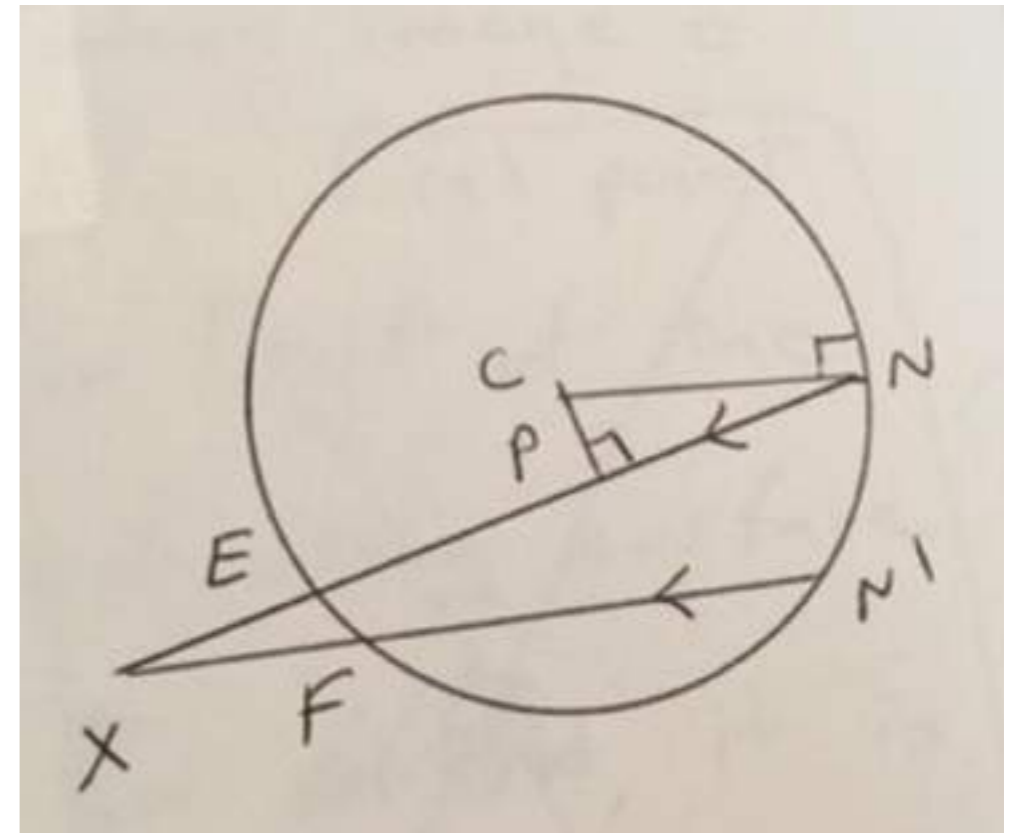


$$\Delta XNN' \cong \Delta XFE$$

$$XE/XN' = EF/NN'$$

$$\begin{aligned} (XE + XN')/2XN' \\ = (EF + NN')/2NN' \end{aligned}$$

Real image at ($X = Z$)
can be projected on a
screen.

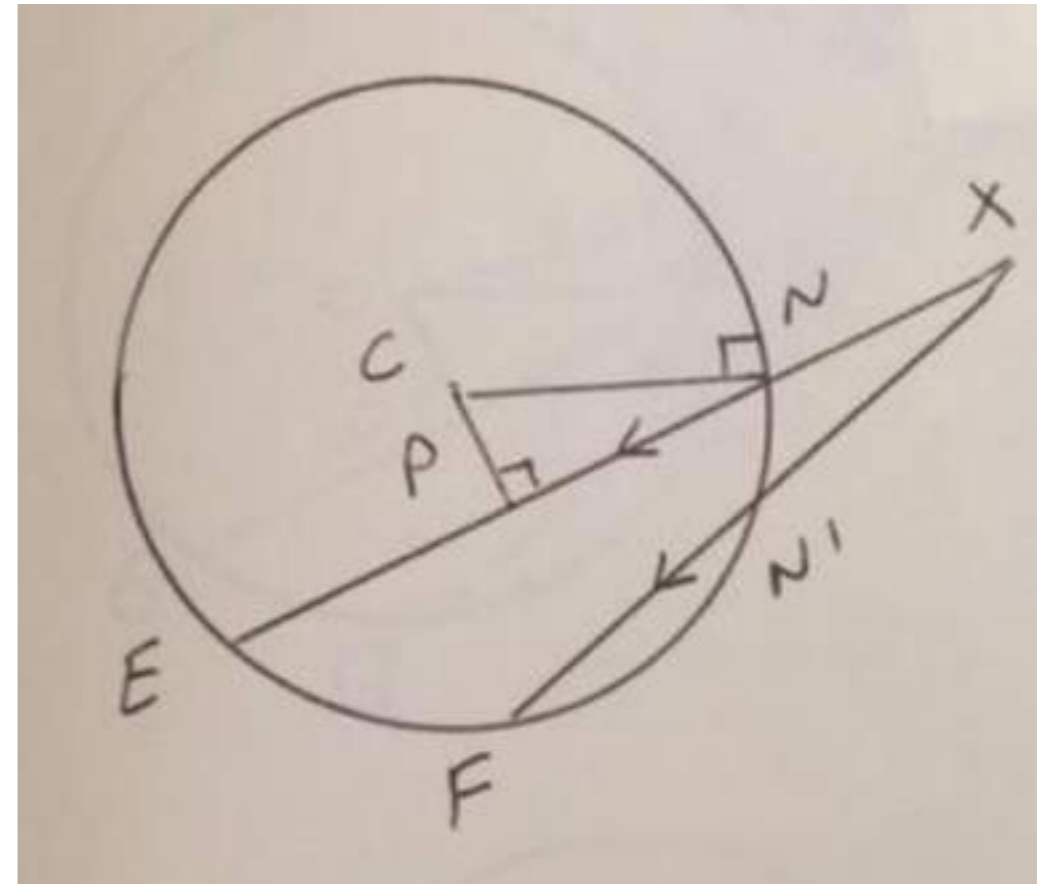


$$\Delta XNN' \cong \Delta XFE$$

$$XE/XN' = EF/NN'$$

$$\begin{aligned} (XE + XN')/2XN' \\ = (EF + NN')/2NN' \end{aligned}$$

Virtual image at ($X = Z$)
can not be projected
on a screen.



$$\begin{aligned} (AG + AN')/2AN' &= (QG + NN')/2NN' \\ (XE + XN')/2XN' &= (EF + NN')/2NN' \end{aligned}$$

$$\begin{aligned} &(QG + NN')/(EF + NN') \\ &= [(AG + AN')/2AN'] [2XN'/(XE + XN')] \end{aligned}$$

As $N' \Rightarrow N$, $X \Rightarrow Z$, and:

$$\begin{aligned} &(\sim QG + \sim NN')/(\sim EF + \sim NN') \\ &\Rightarrow (QG + NN')/(EF + NN') \\ &\Rightarrow (AO/AN)(ZN/ZP) \end{aligned}$$

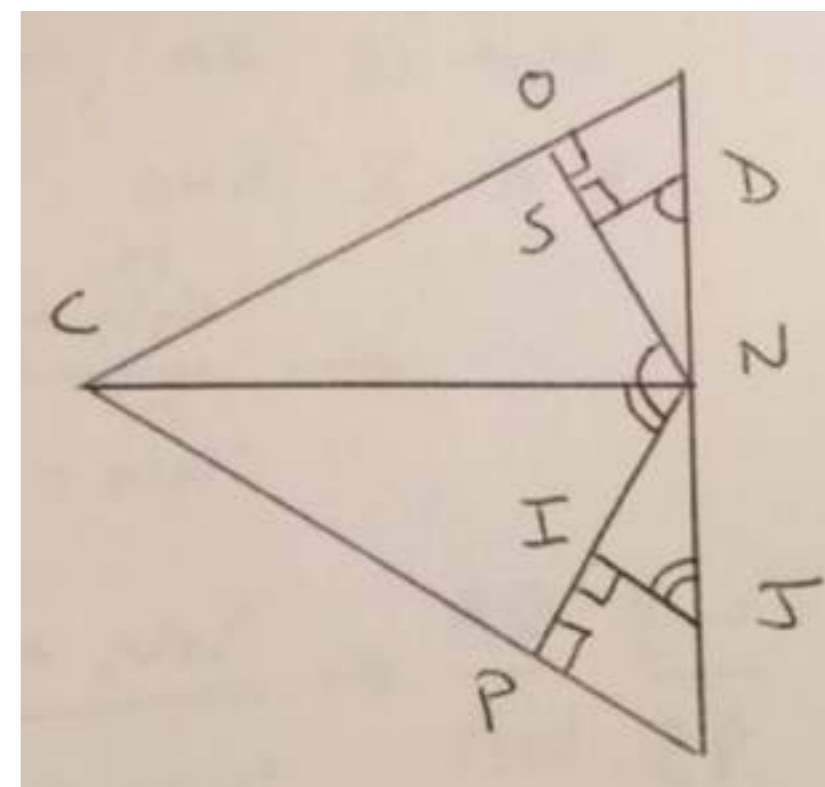
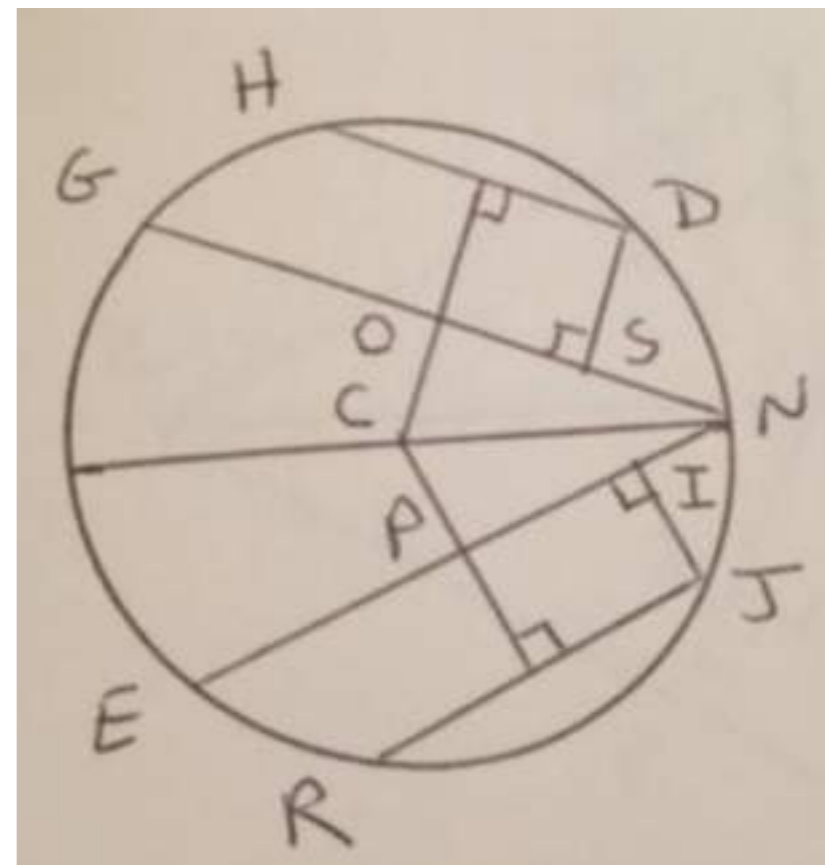
Also, when $HD = QN'$
and $RJ = FN'$

$$\begin{aligned} & (\sim QG + \sim NN') / (\sim EF + \sim NN') \\ & = 2(\sim ND) / 2(\sim NJ) = \sim ND / \sim NJ \end{aligned}$$

As $N' \Rightarrow N$, $X \Rightarrow Z$, and:

$\sim DJ \Rightarrow$ line segment DJ , so:

$$\begin{aligned} & (\sim QG + \sim NN') / (\sim EF + \sim NN') \\ & \Rightarrow ND / NJ \end{aligned}$$



DS/JI = CO/CP

JI/JN = NP/NC

DN/DS = NC/NO

ND/NJ = (NP/NO)(CO/CP)

As $N' \Rightarrow N$, $X \Rightarrow Z$, and:

$(\sim QG + \sim NN') / (\sim EF + \sim NN')$

$\Rightarrow (NP/NO)(CO/CP)$

and therefore:

$(AO/AN)(ZN/ZP) \Rightarrow (NP/NO)(CO/CP)$

Thus $R = CO/CP$, and Z , (along both NP and CW), is the clear image of A refracted along $\sim BN$, when:

$NT \parallel CO$, so:

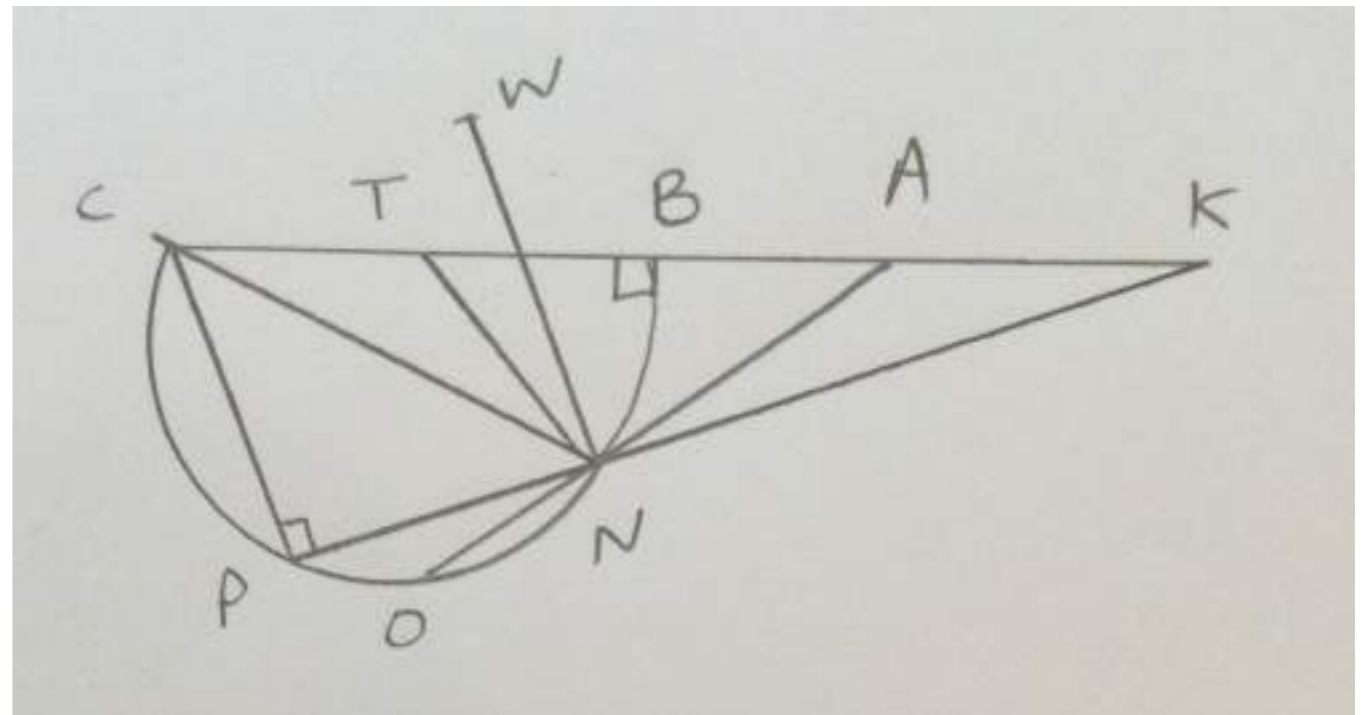
$AO/AN = CO/NT$ and:

$NW \parallel CP$, so:

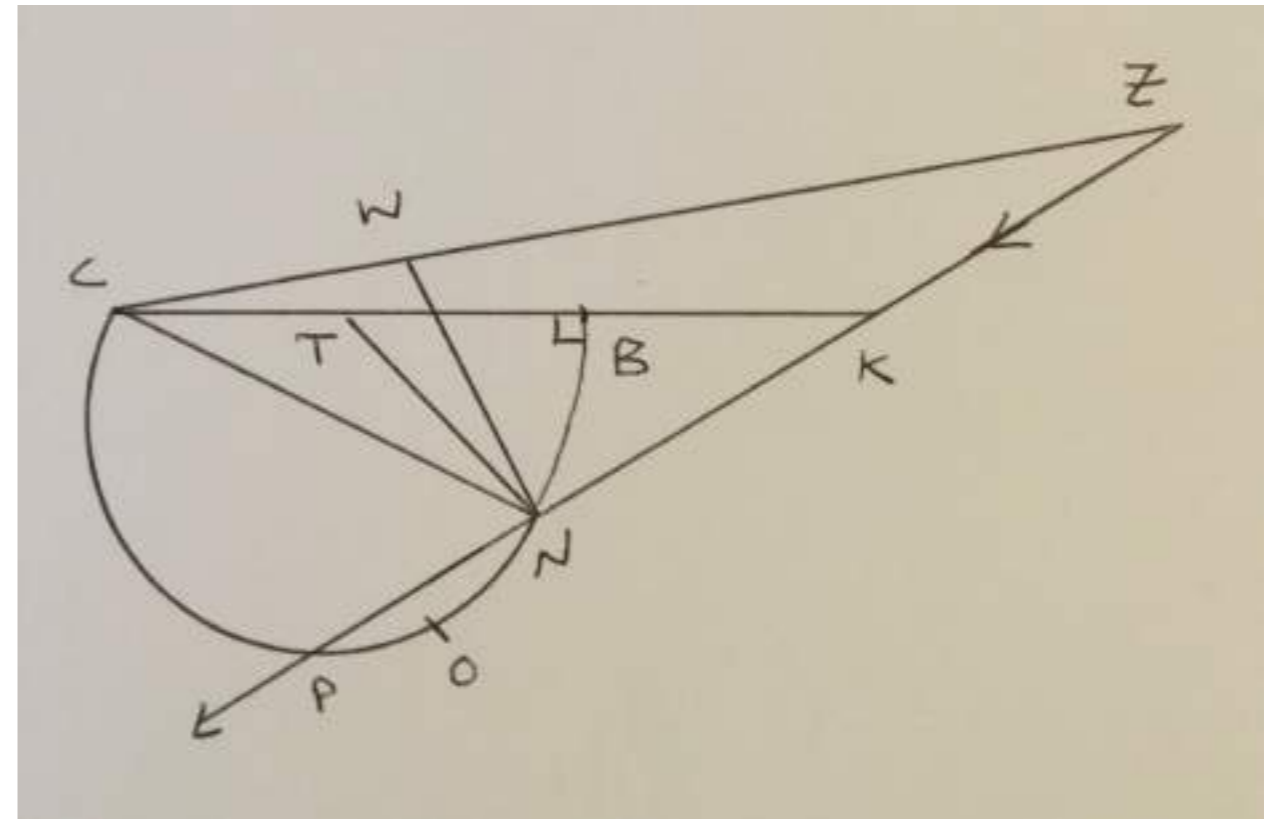
$ZN/ZP = NW/CP$ and:

$NW/NT = NP/NO$

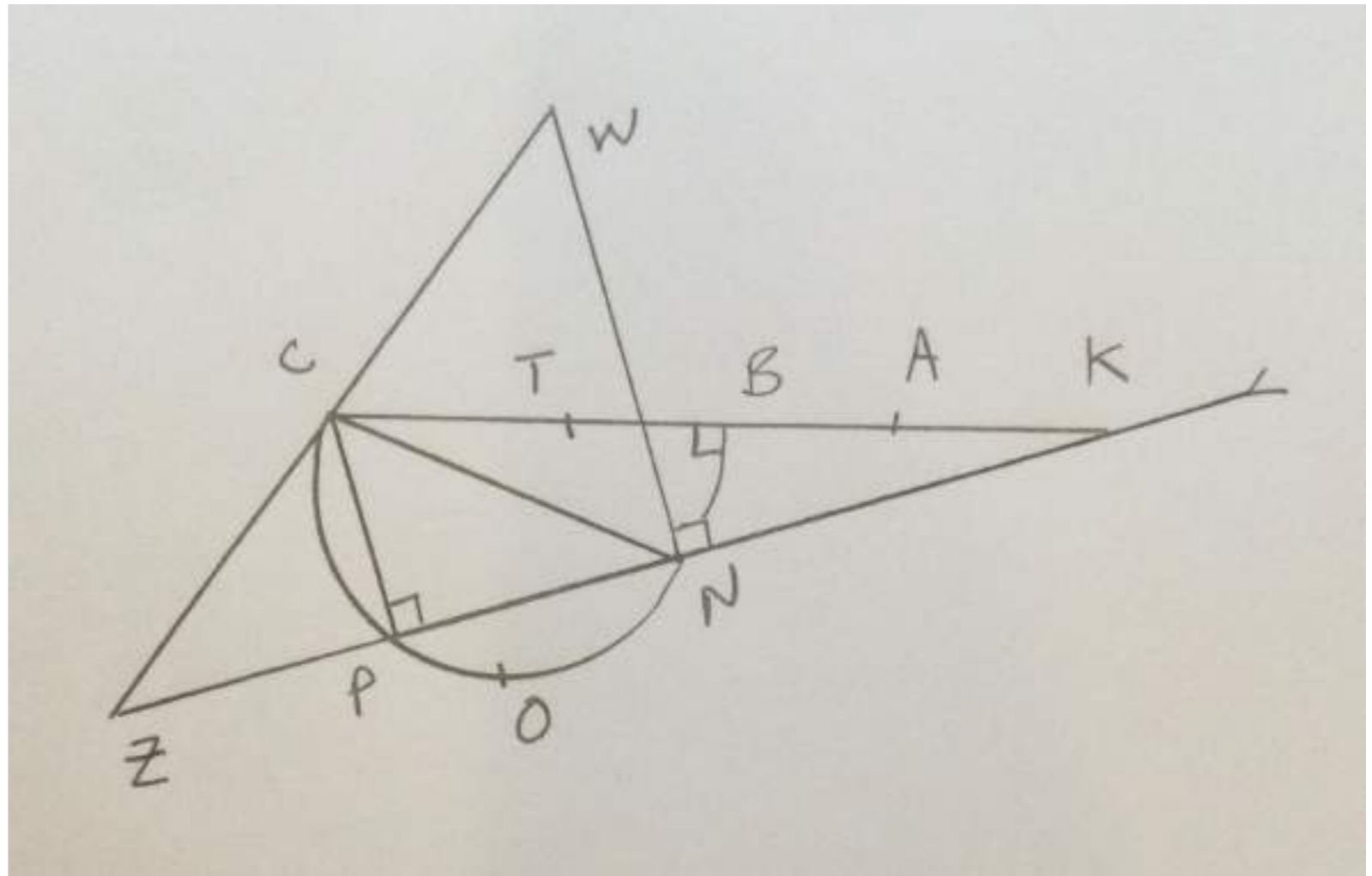
$(\triangle WNT \cong \triangle PNO)$



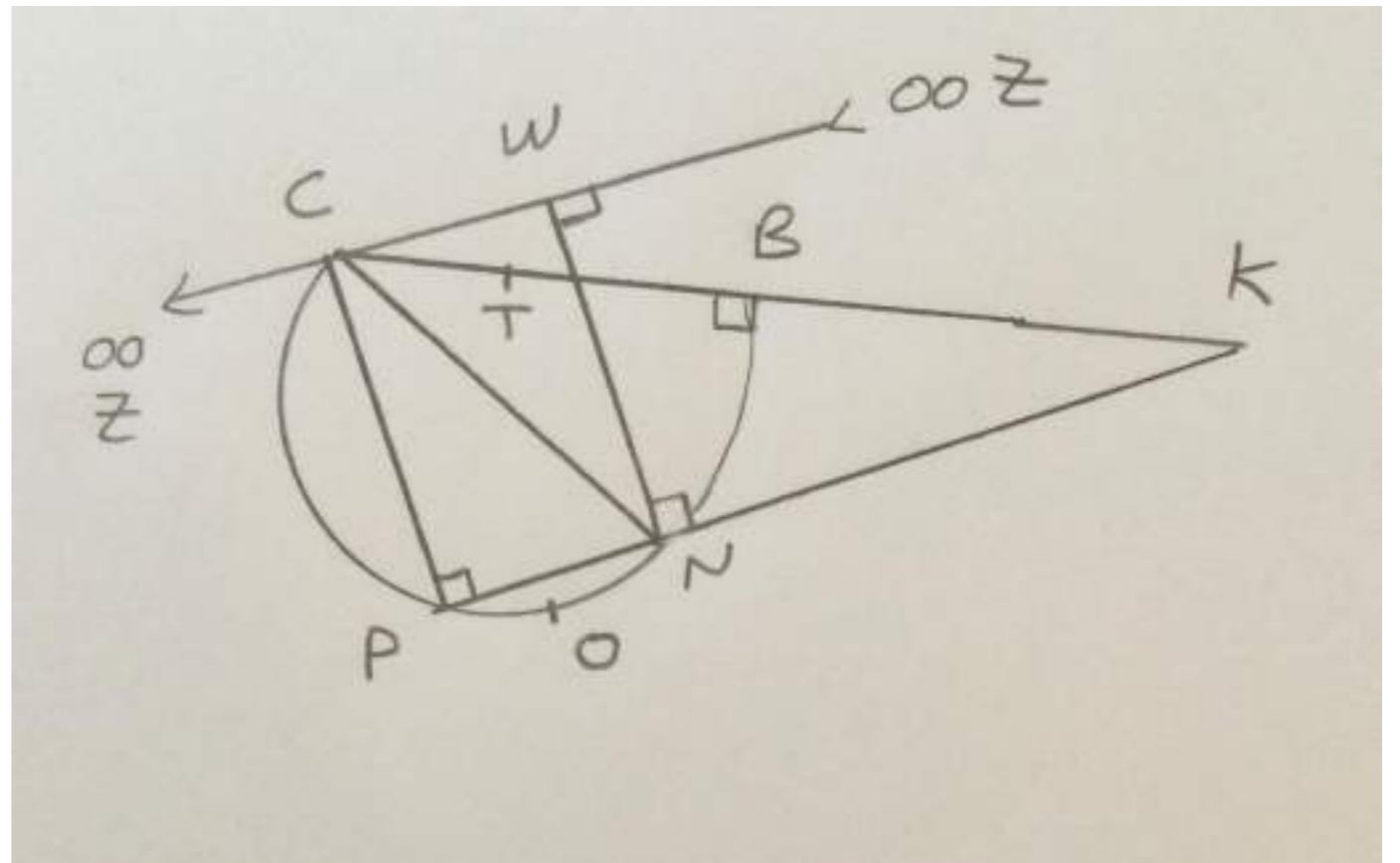
The off-axis rays from any on-axis object A, (real or virtual), can not form a virtual on-axis image at Z because NW must be less than CP for Z to be virtual; but NW must also be greater than NT.



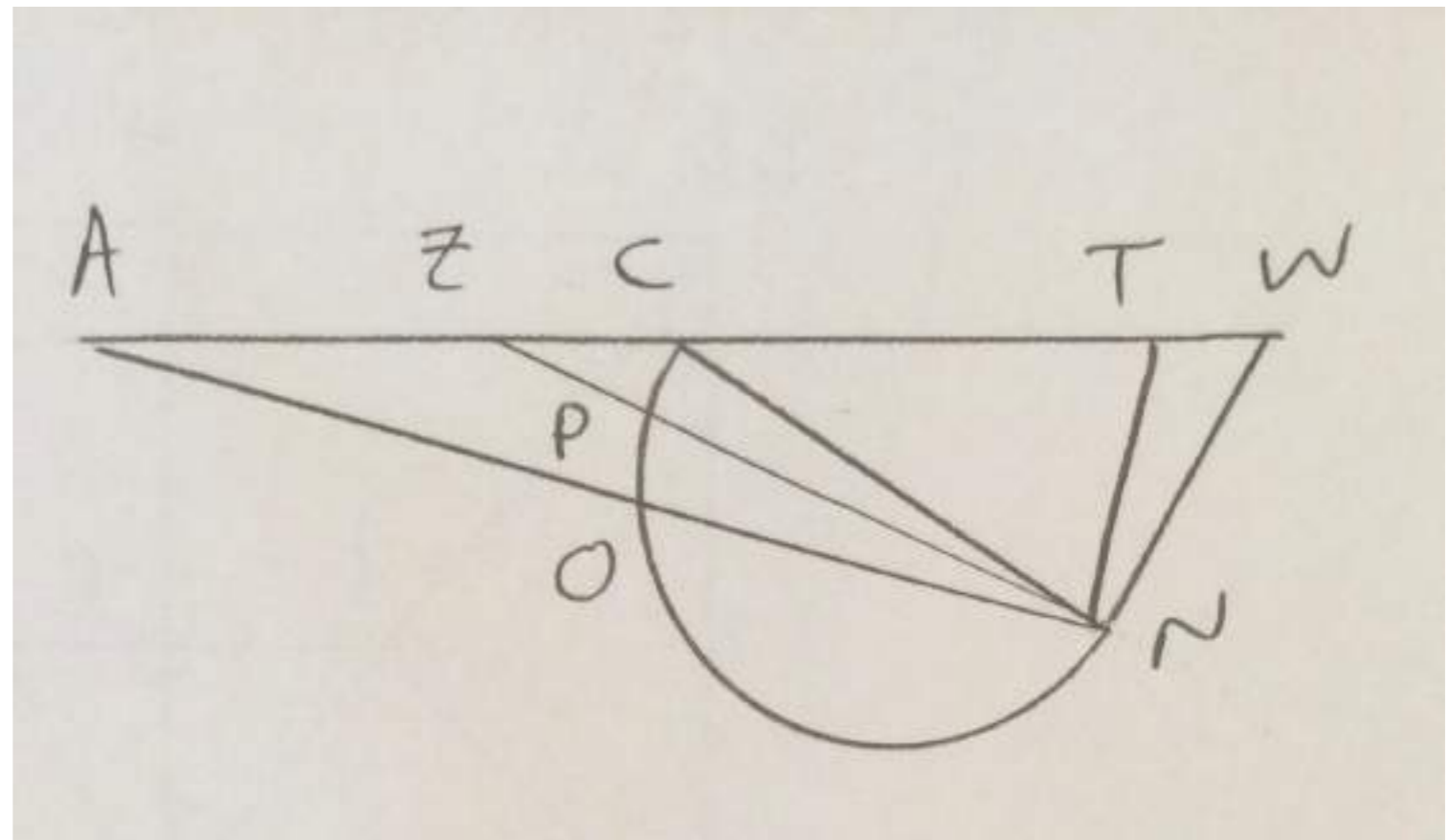
The off-axis rays from any real on-axis object A can not form a real on-axis image at Z because NW must be greater than (or equal to) CP for Z to be real; but NW must also be greater than NT.



The off-axis rays from any real on-axis object A can not form a real on-axis image at Z because NW must be greater than (or equal to, as shown here) CP for Z to be real; but NW must also be greater than NT.



The off-axis rays from a virtual on-axis object A **can** form a real on-axis image at Z , if NW is greater than CP , and WT lies along the axis.



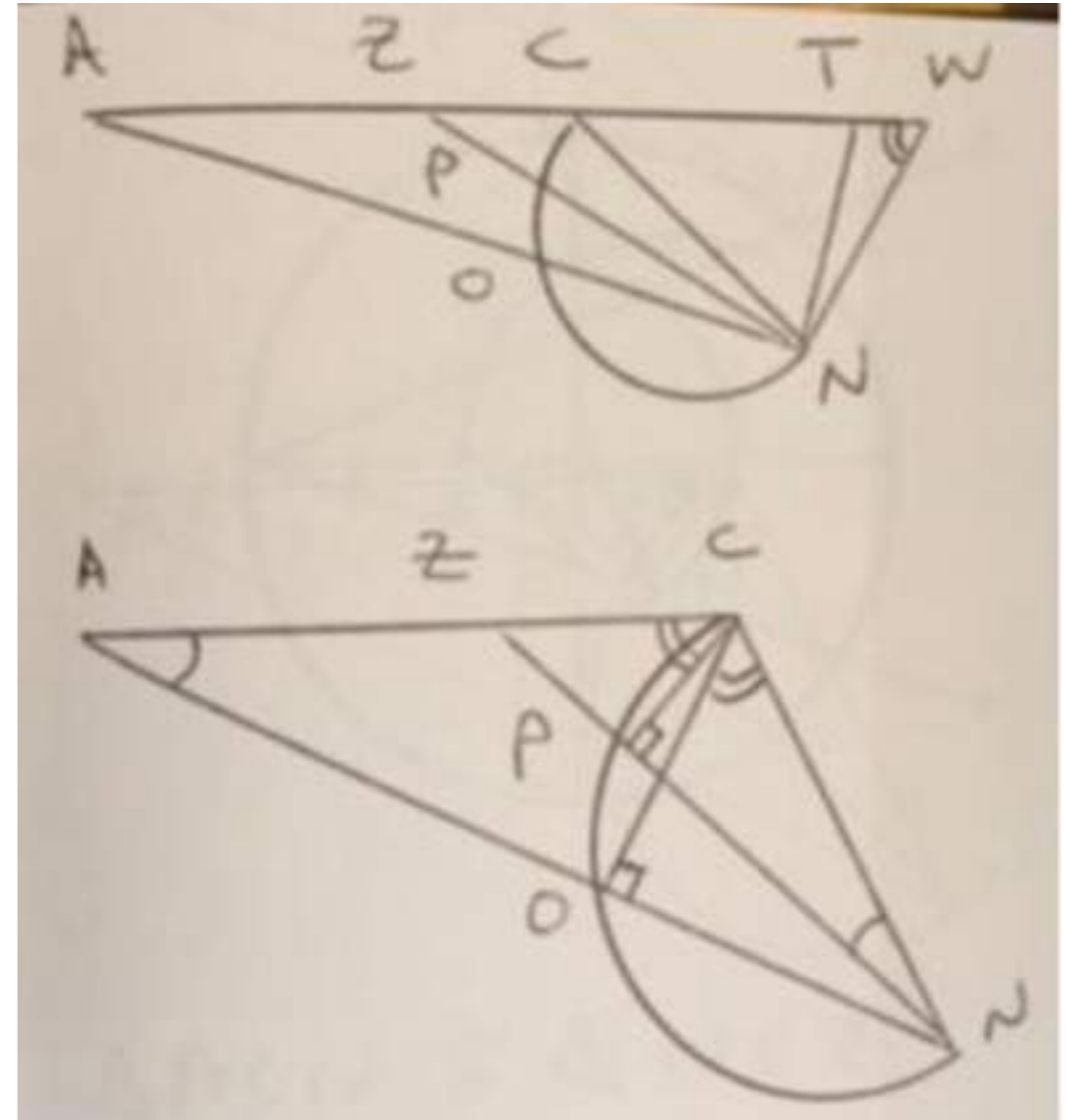
Since:

$$\angle NWT = \angle NPO = \angle NCO$$

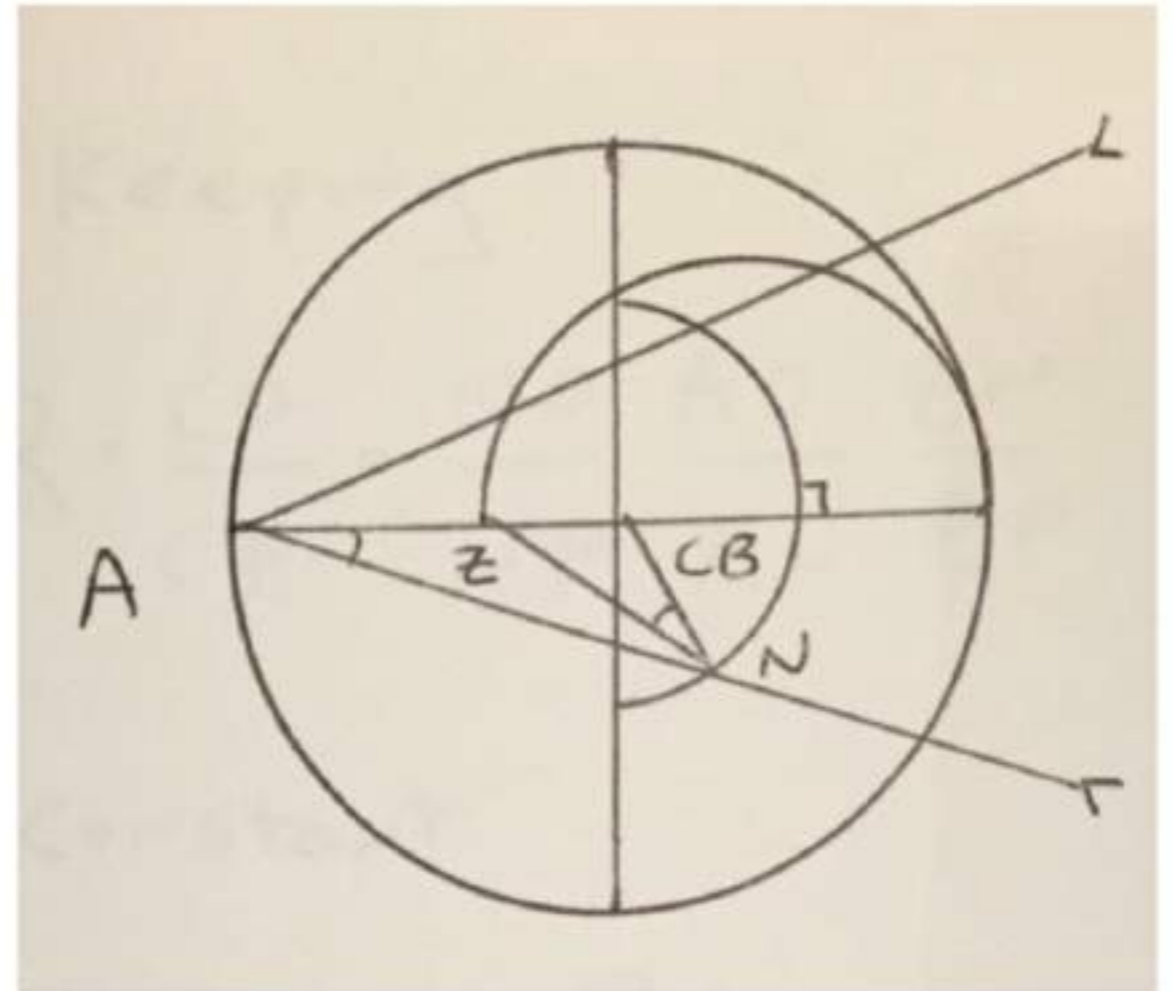
and $NW \parallel CP$

WT lies along the axis when:

$$\triangle NCO \cong \triangle ZCP$$



When off-axis rays from a virtual on-axis object A form a real on-axis image Z , this occurs at all points N because:



$$\triangle ACN \cong \triangle NCZ \text{ for all } N$$

4). refraction through a circle's center

Keeping:

$$\mathbf{R} = (\text{CO/CP}) = (\text{NO/NP})(\text{AO/AN})(\text{ZN/ZP})$$

constant as:

$$\text{N} \Rightarrow \text{B:}$$

$$(\text{BC/BC})(\text{AC/AB})(\text{ZB/ZC}) \Rightarrow \mathbf{R}$$

Refraction through a circle's center occurs when N lies at B, so that an object's ray from A to N lies along ABC, and an image ray lies along BCZ. The locations of the object A and image Z along the optic axis BC are described by the equation:

$$R = CO/CP = (AC/AB)(ZB/ZC)$$

If we draw A and Z along the optic axis BC **as if** it were a circle, and draw CDL so that $AL \parallel ZB$:

$\Delta ACB \cong \Delta ZCD$, and:

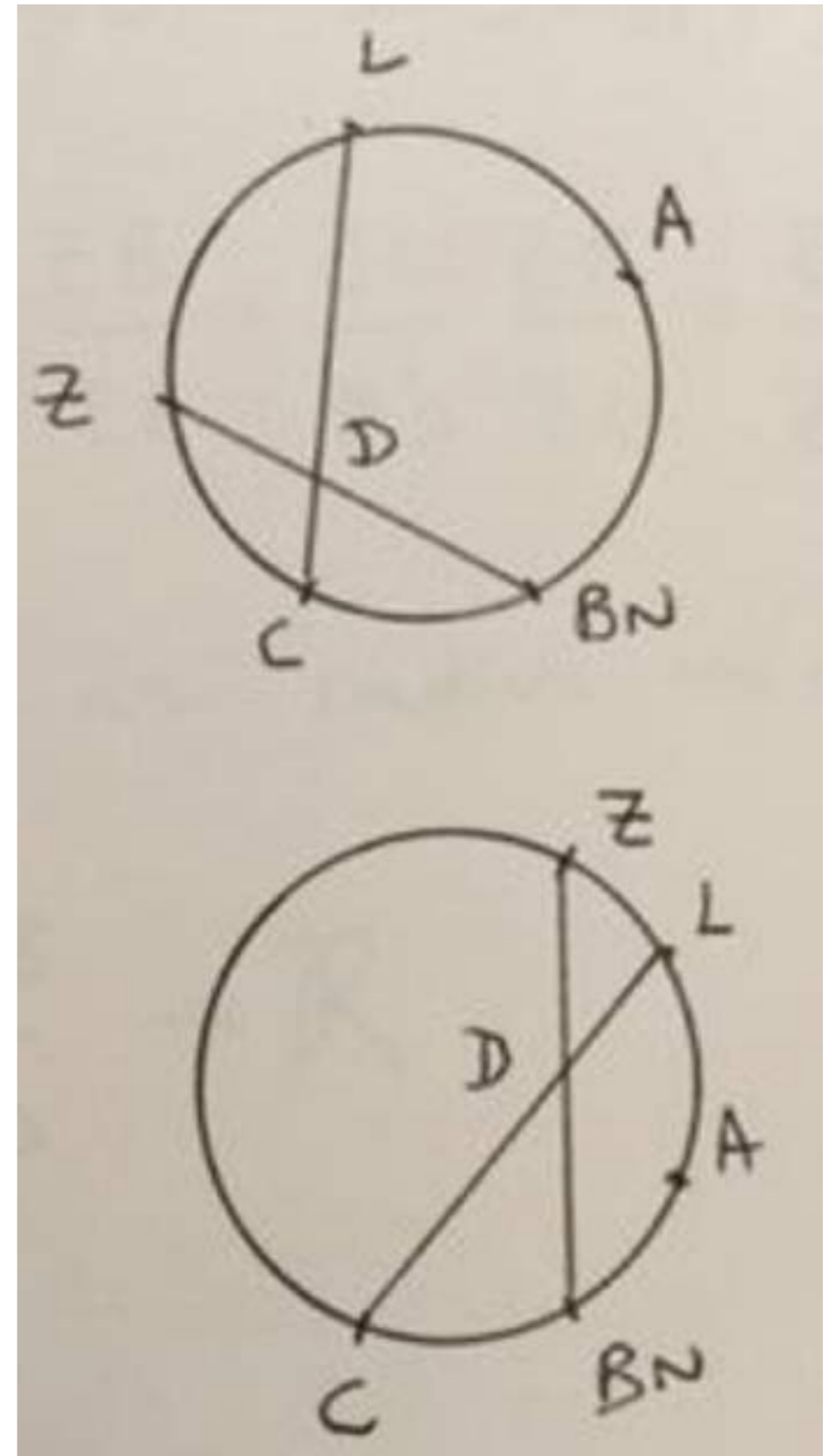
$$(AC/AB)(ZB/ZC) =$$

$$(ZC/ZD)(ZB/ZC) =$$

$$(ZB/ZD)$$

so as the reference circle's radius $\Rightarrow \infty$

$$(ZB/ZD) \Rightarrow \mathbf{R}$$



$AL \parallel ZB$

$AZ = BL$

$\sim AZ = \sim BL$

$HZ \parallel CL$

$ZC = LJ$

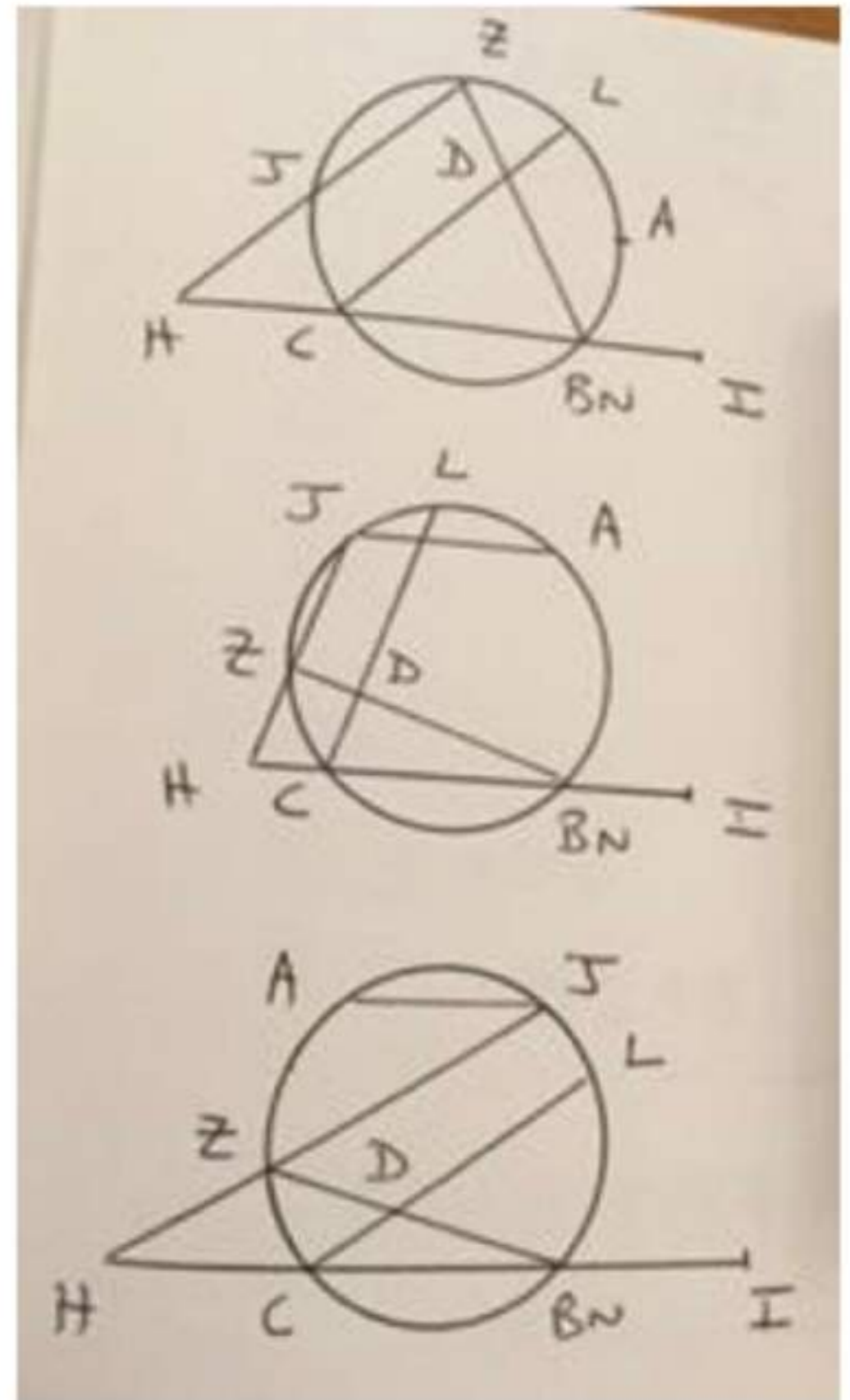
$\sim ZC = \sim LJ$

$\sim AZ + \sim ZC = \sim AZC$

$\sim BL + \sim LJ = \sim BLJ$

$\sim AZC = \sim BLJ$

$AJ \parallel CB$



$HZ \parallel CL$

$$ZB/ZD = HB/HC$$

$$\Delta HBZ \cong \Delta HJC$$

when $\Delta HJC = \Delta IAB$:

$$HC = IB, \text{ and:}$$

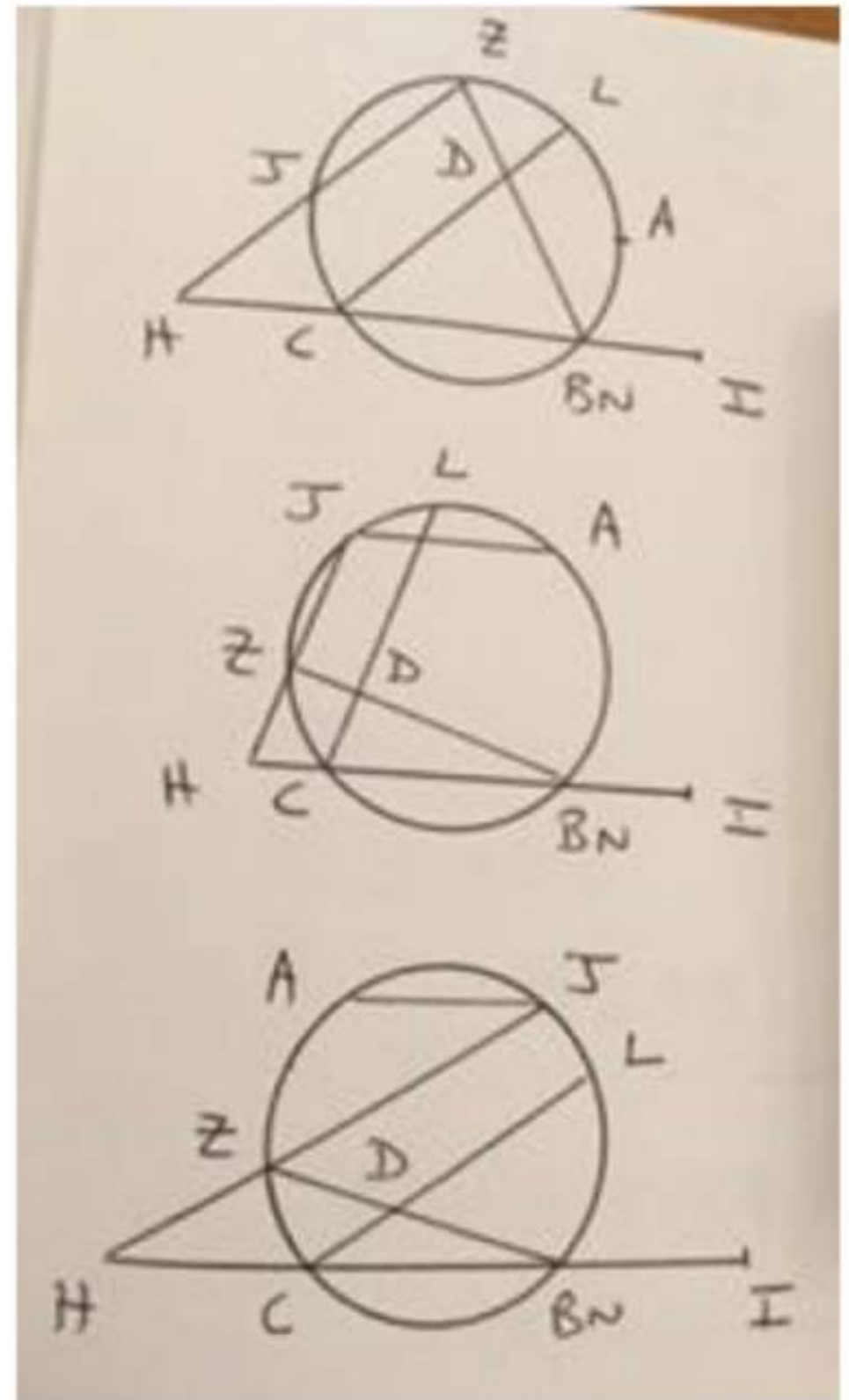
$$IB/IA = HZ/HB$$

This results in

Newton's Equation

as the reference circle's
radius $\Rightarrow \infty$:

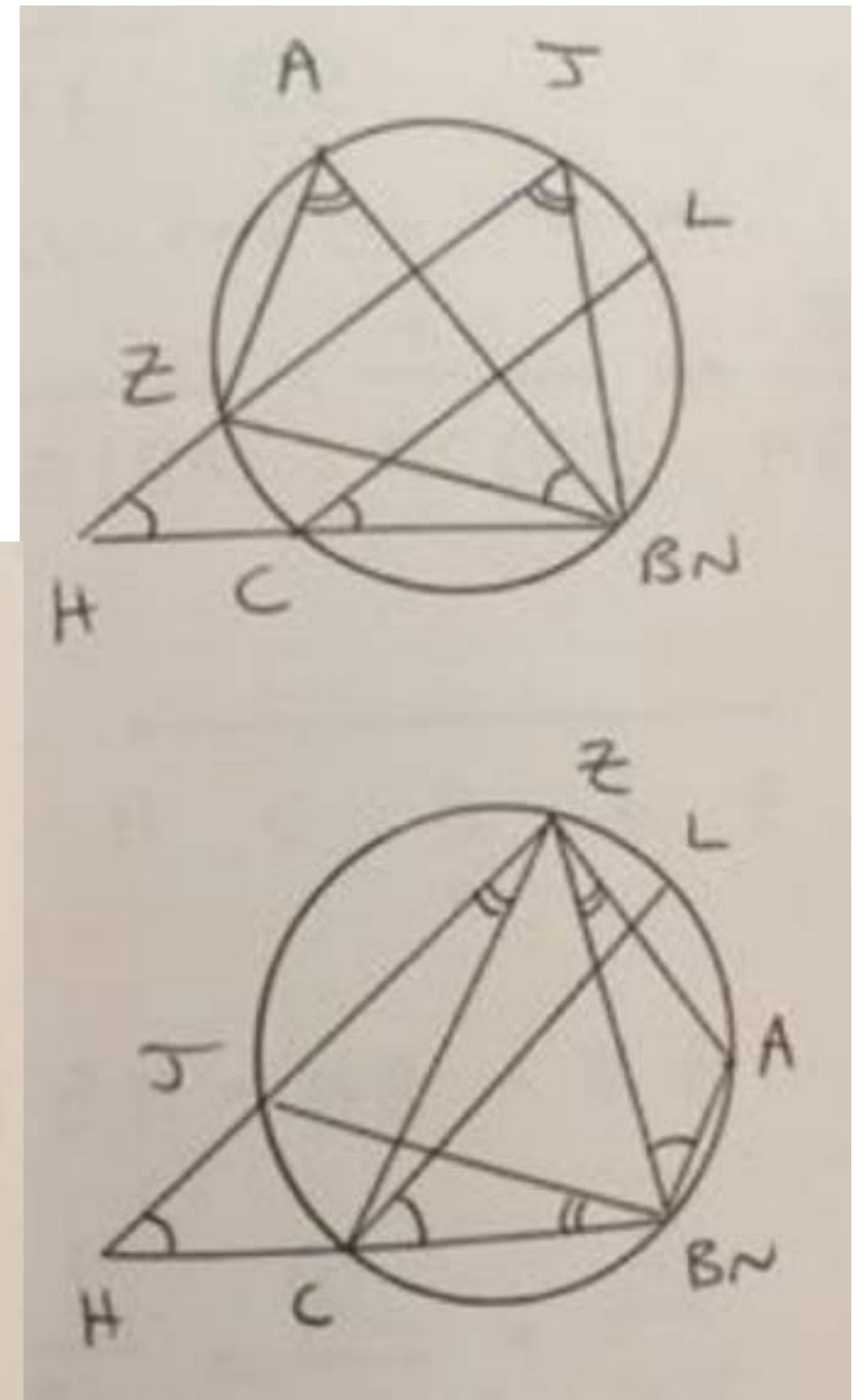
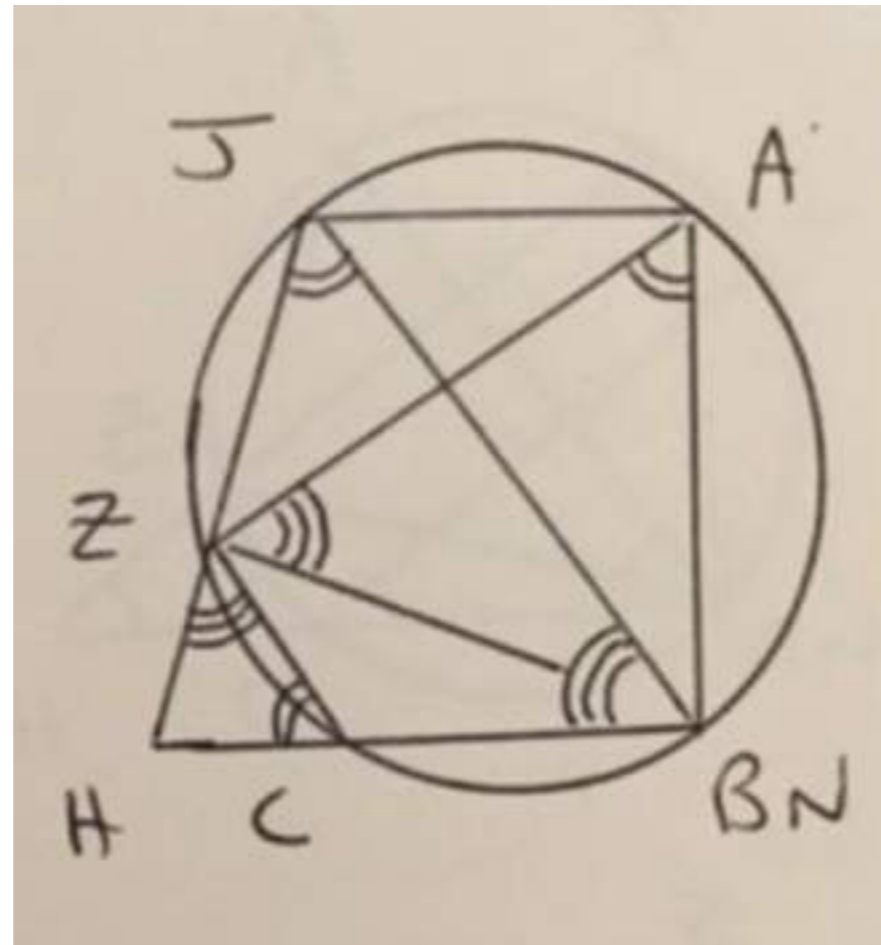
$$(AI)(ZH) = (BI)(BH)$$



$$\Delta HCZ \cong \Delta HJB \cong \Delta BAZ$$

$$(HC/HZ) = (BA/BZ)$$

$$[1/(HZ)(BA)] = [1/(HC)(BZ)]$$



as the reference circle's radius $\Rightarrow \infty$:

$$[1/(HZ)(BA)] = [1/(HC)(BZ)] \Rightarrow \mathbf{R}/(HB)(BZ)$$

and the resulting possible sums occur:

$$HZ = HB + BZ$$

$$HB = HZ + BZ$$

$$BZ = HZ + HB$$

which, when multiplied by the above three factors, form the **conjugate foci equations**.

The conjugate foci equations allow for the effect of axial refraction at a circle to be expressed as the term:

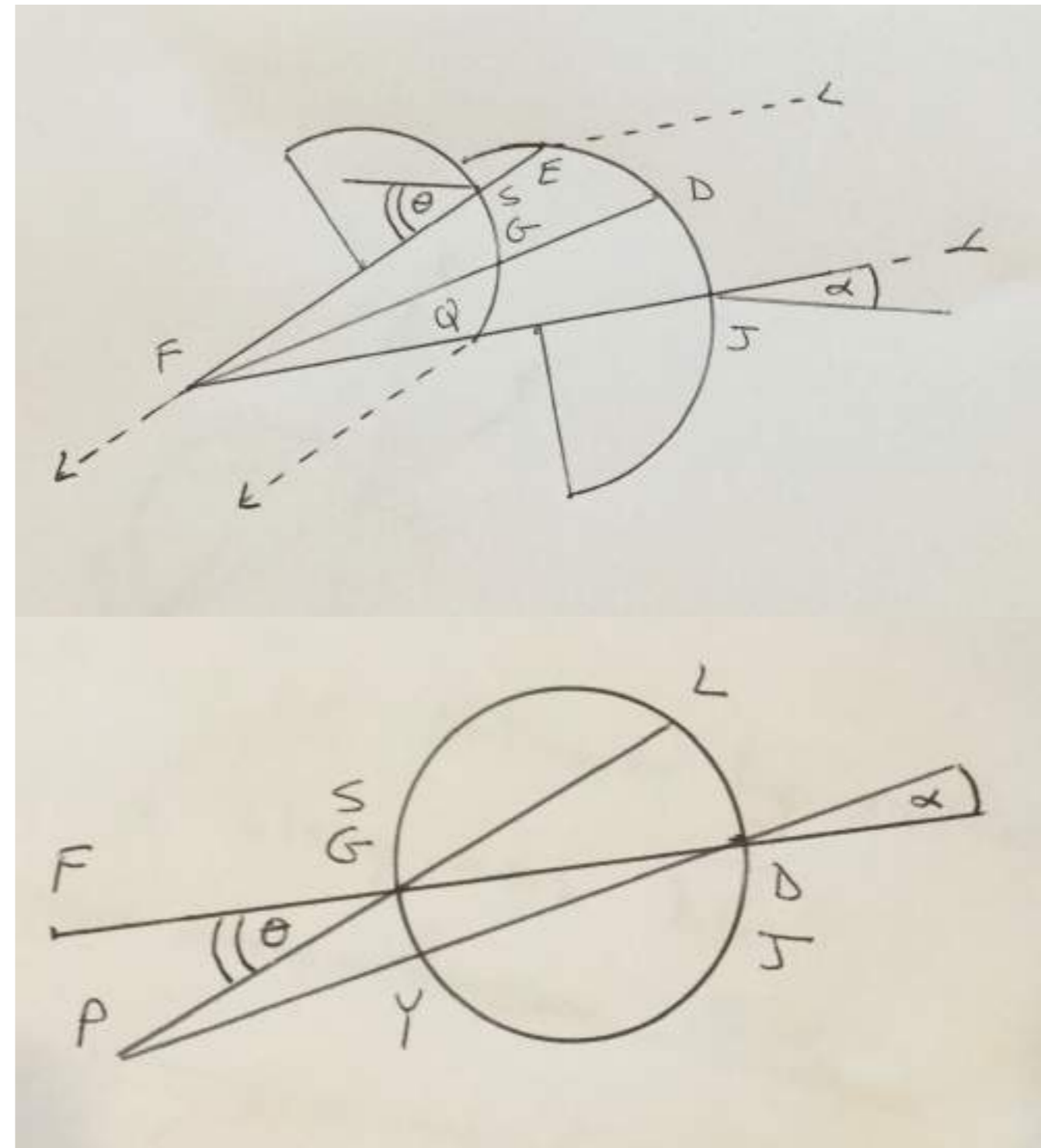
$$(1/HC) = (\mathbf{R}/HB)$$

which is then additive with object vergence, defined as $(1/BA)$; or image vergence, defined as (\mathbf{R}/BZ) .

5). afocal angular magnification/minification

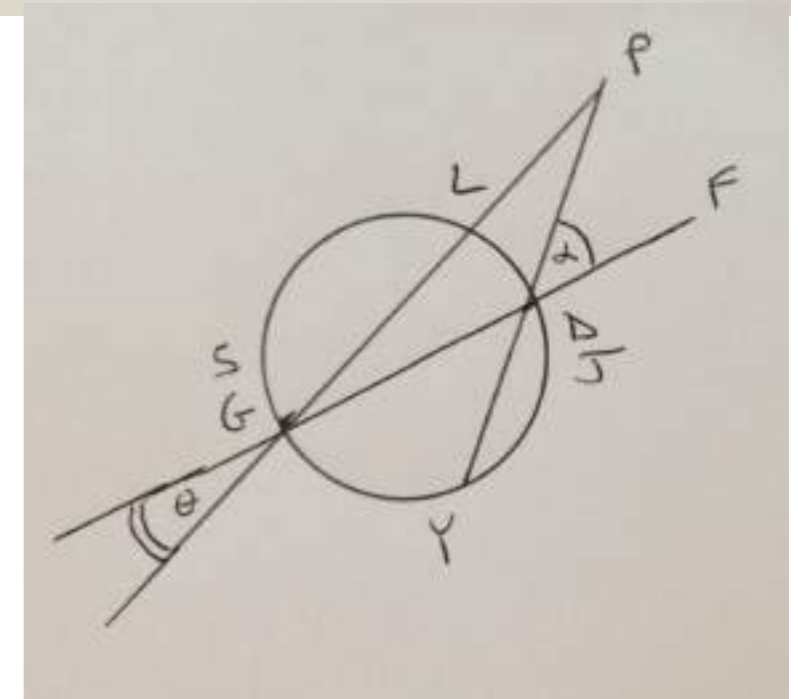
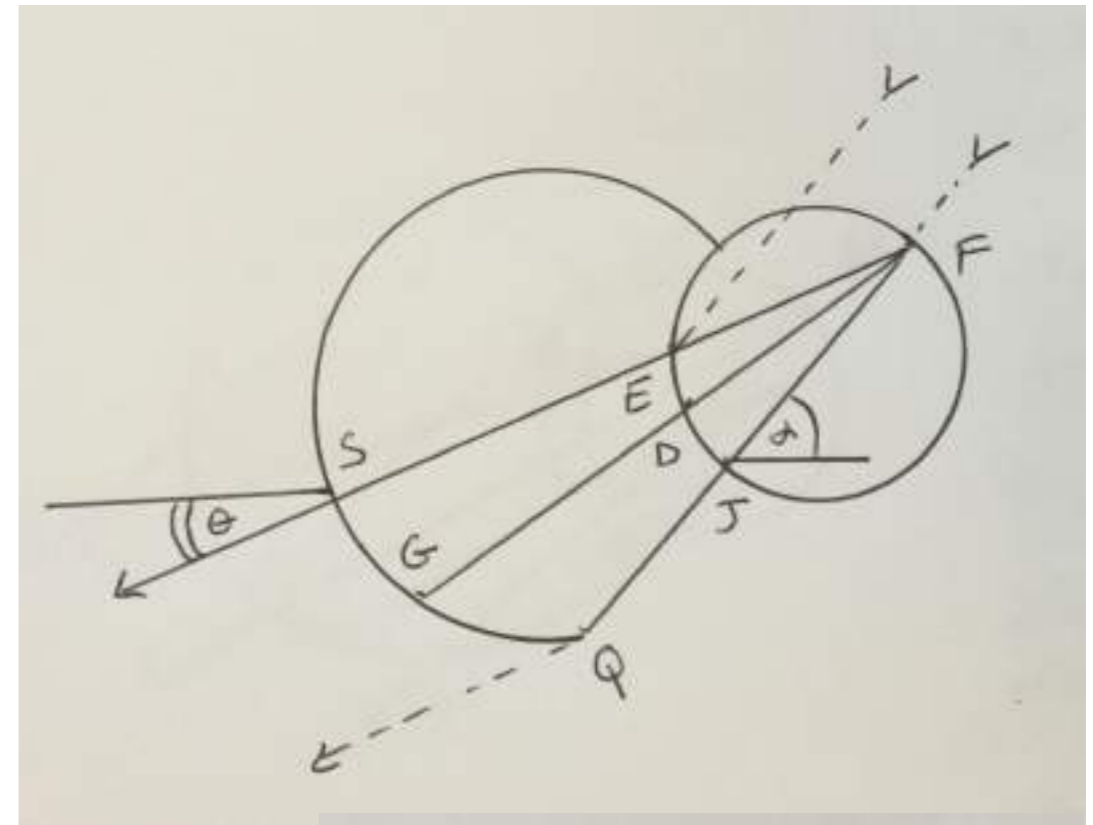
Afocal Angular Magnification

When distance refraction at $\sim JDE$ is followed by refraction into distance at $\sim QGS$ along axis DGF as shown;
as $\angle JFD = \angle SFG$,
and both approach zero:



Afocal Angular Minification

Or when distance refraction at $\sim JDE$ is followed by refraction into distance at $\sim QGS$ along axis FDG , as shown; as $\angle JFD = \angle SFG$, and both approach zero:



$$\theta/\alpha \Rightarrow (\sim LD/GD)/(\sim YG/GD) \text{ as } P \Rightarrow F$$

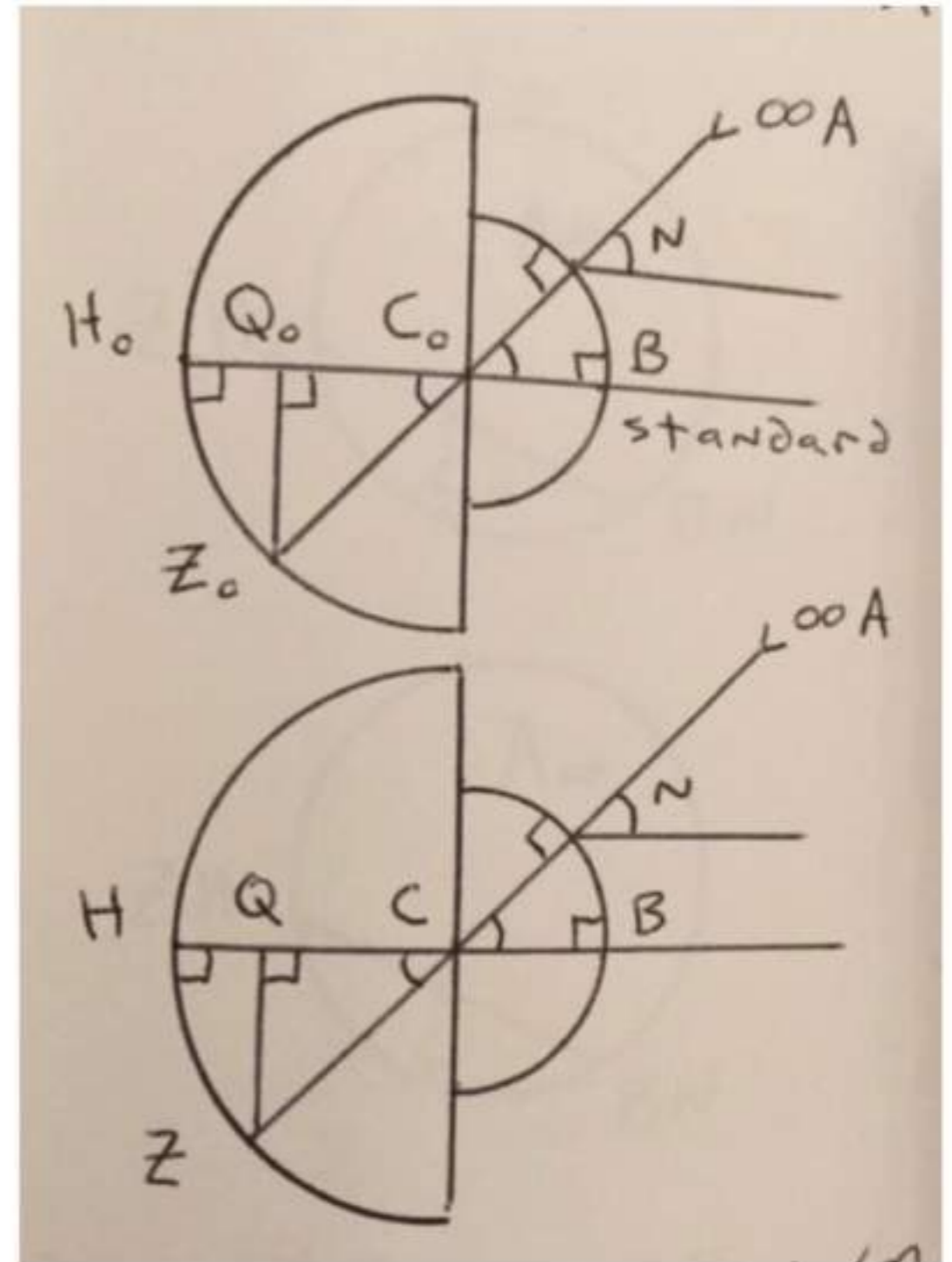
$$\theta/\alpha \Rightarrow (FD/FG) \text{ as } P \Rightarrow F$$

so that **afocal axial angular magnification/minification** equals:

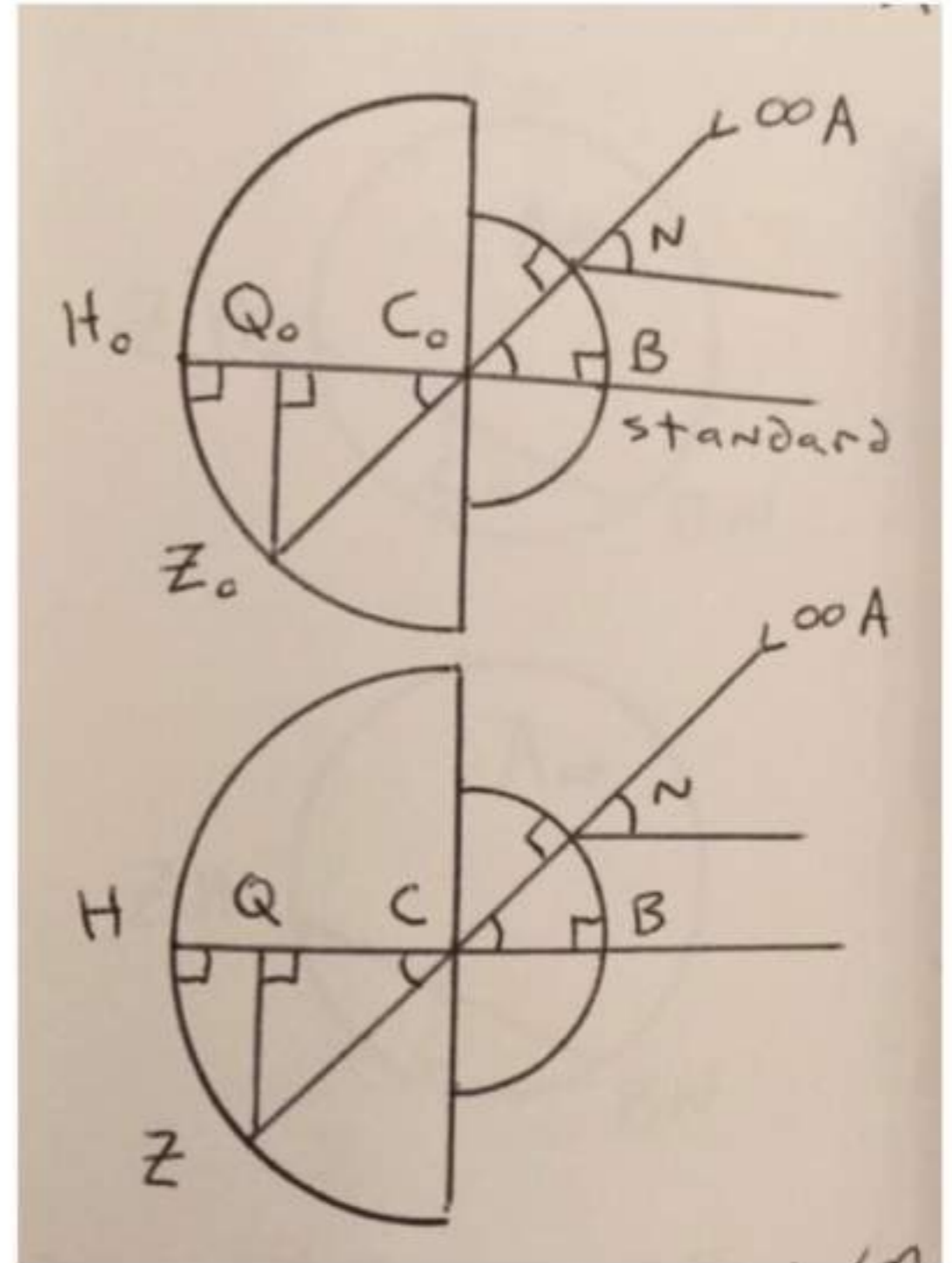
$$FD/FG$$

6). retinal image size magnification

The top diagram illustrates a standard single-surfaced eye with a distant object A, and resulting retinal image size H_oZ_o .



The bottom diagram illustrates any single-surfaced eye with a distant object A, and resulting retinal image size HZ.

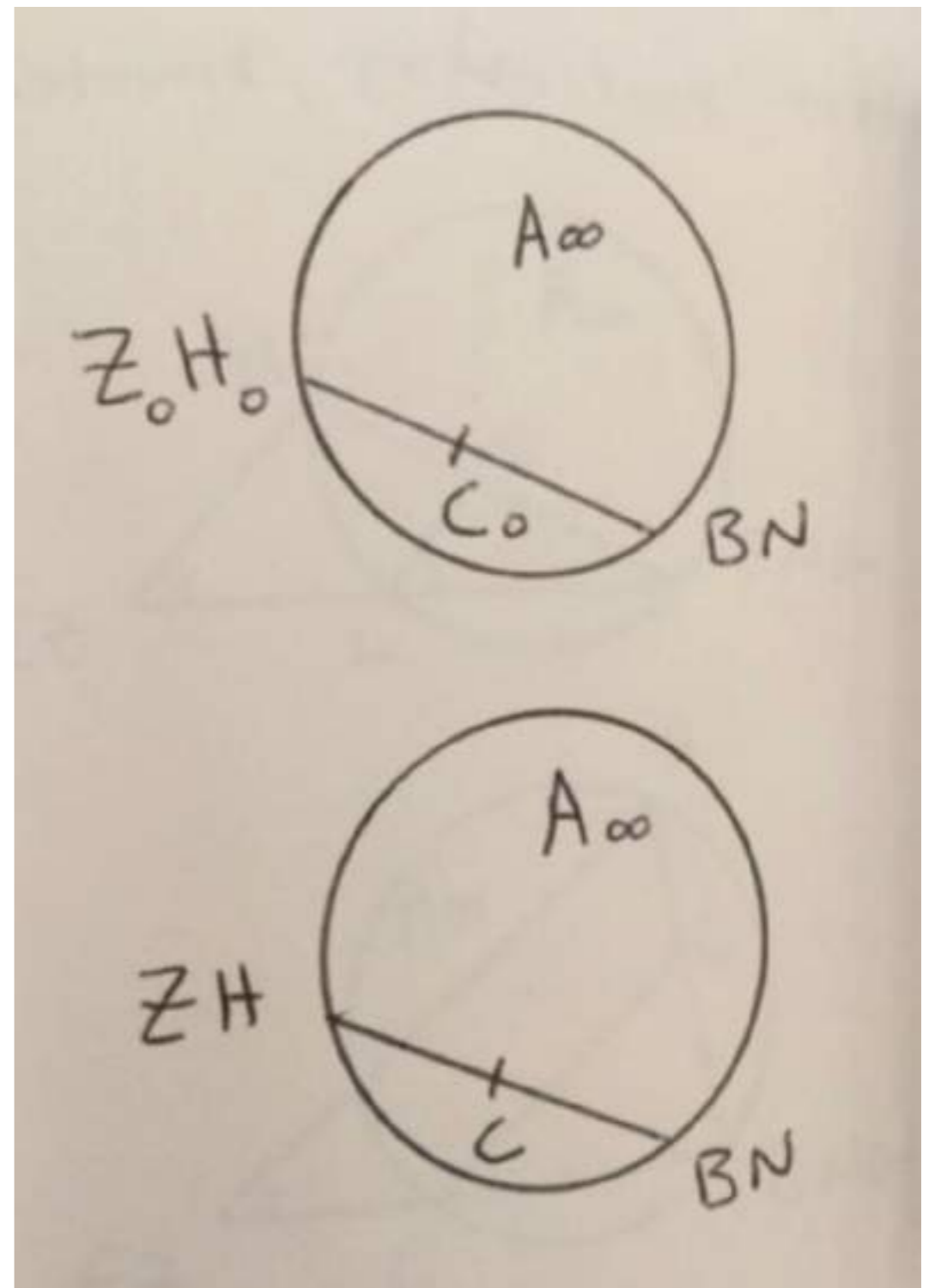


As $N \Rightarrow B$, the retinal image size magnification, ZH/Z_oH_o , (relative to an arbitrary standard which factors out with subsequent comparisons), then approaches its axial value:

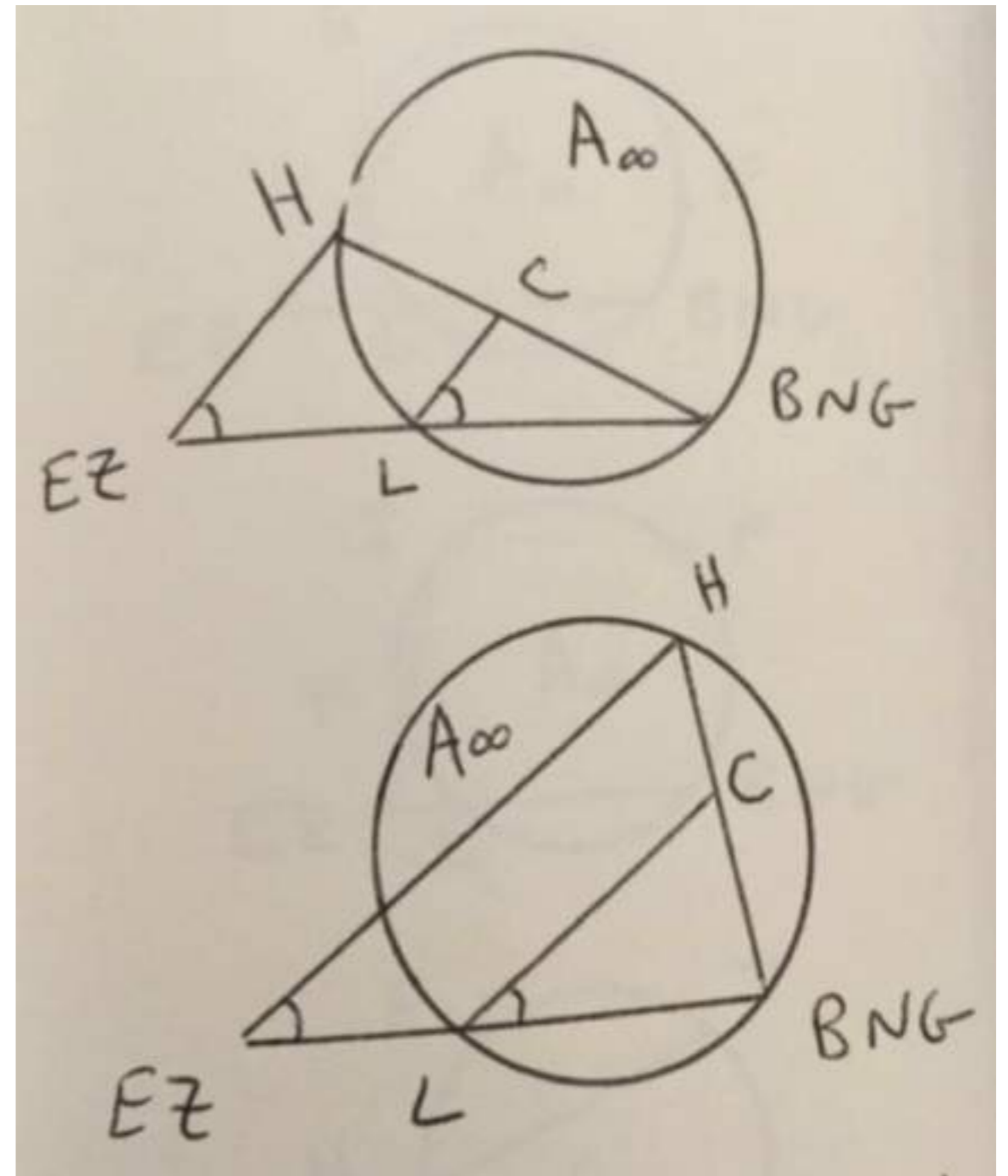
$$\begin{aligned} ZQ/Z_oQ_o &= ZC/Z_oC_o = HC/H_oC_o \\ &= (BH/\mathbf{R})/(BH_o/\mathbf{R}) = BH/BH_o \end{aligned}$$

7). axial magnification of distance correction

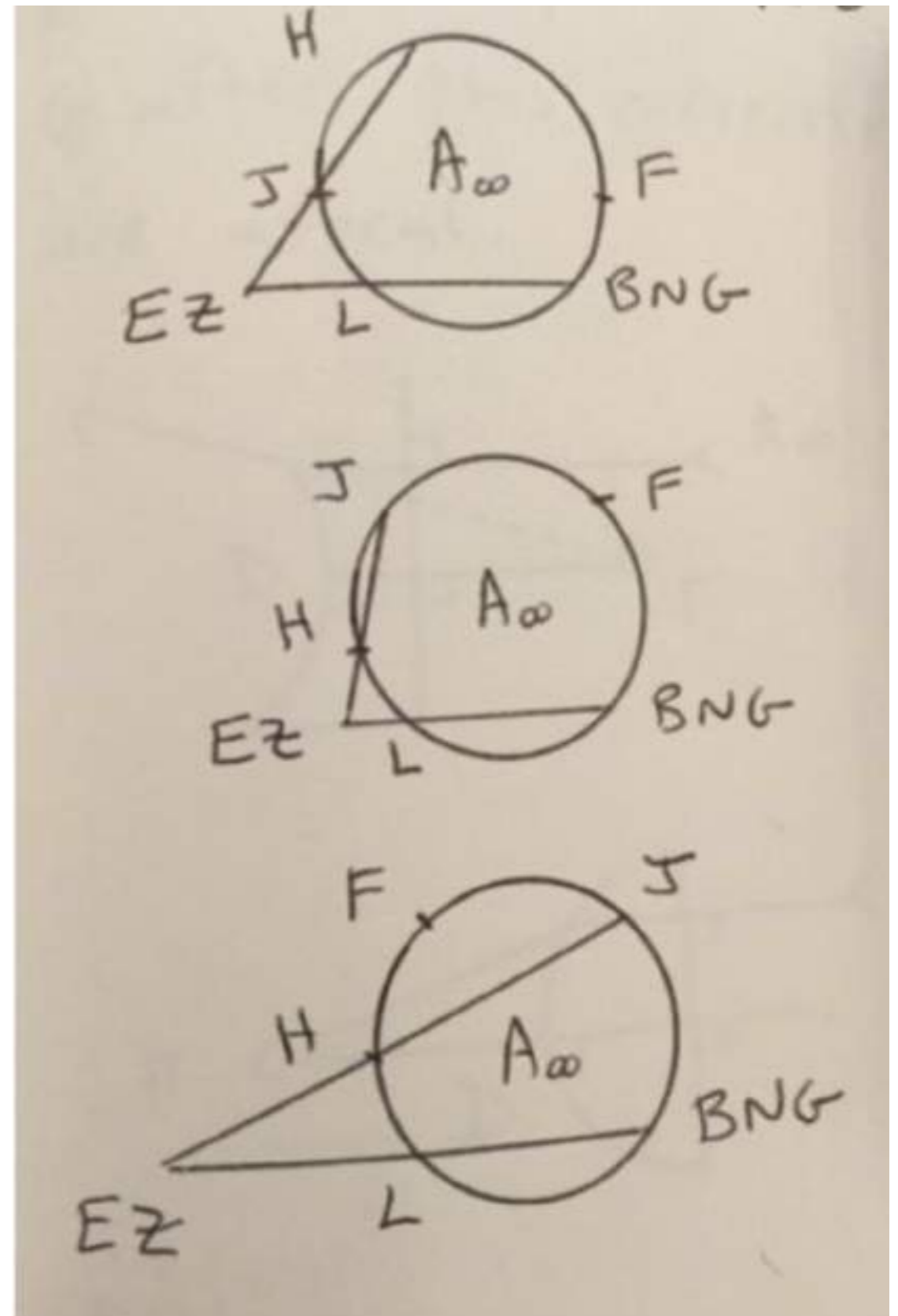
Once again representing the optic axis BCZ as a circle of infinite radius, the distant object A is focused by the curve of radius BC towards the axial object Z, (which lies at the retina H when there is no distance refractive error).



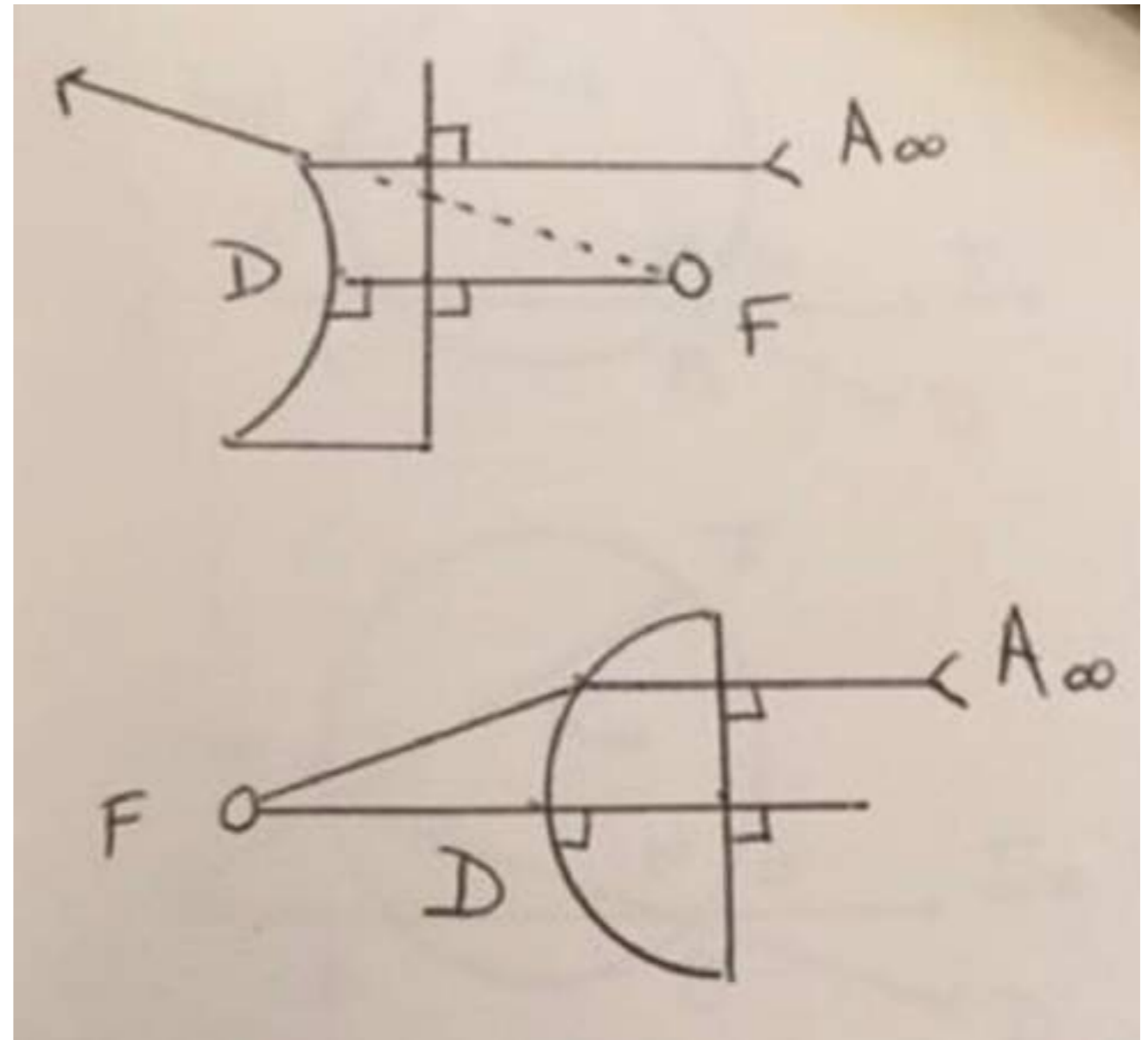
additional
refraction at G (at
B) will create
distance refractive
error and a
combined single
refractive surface
of radius BL .



A distance correction must focus the distant object A towards the focal point F of the refractive error G, so that $JF \parallel BE$, in order to move Z back to H.

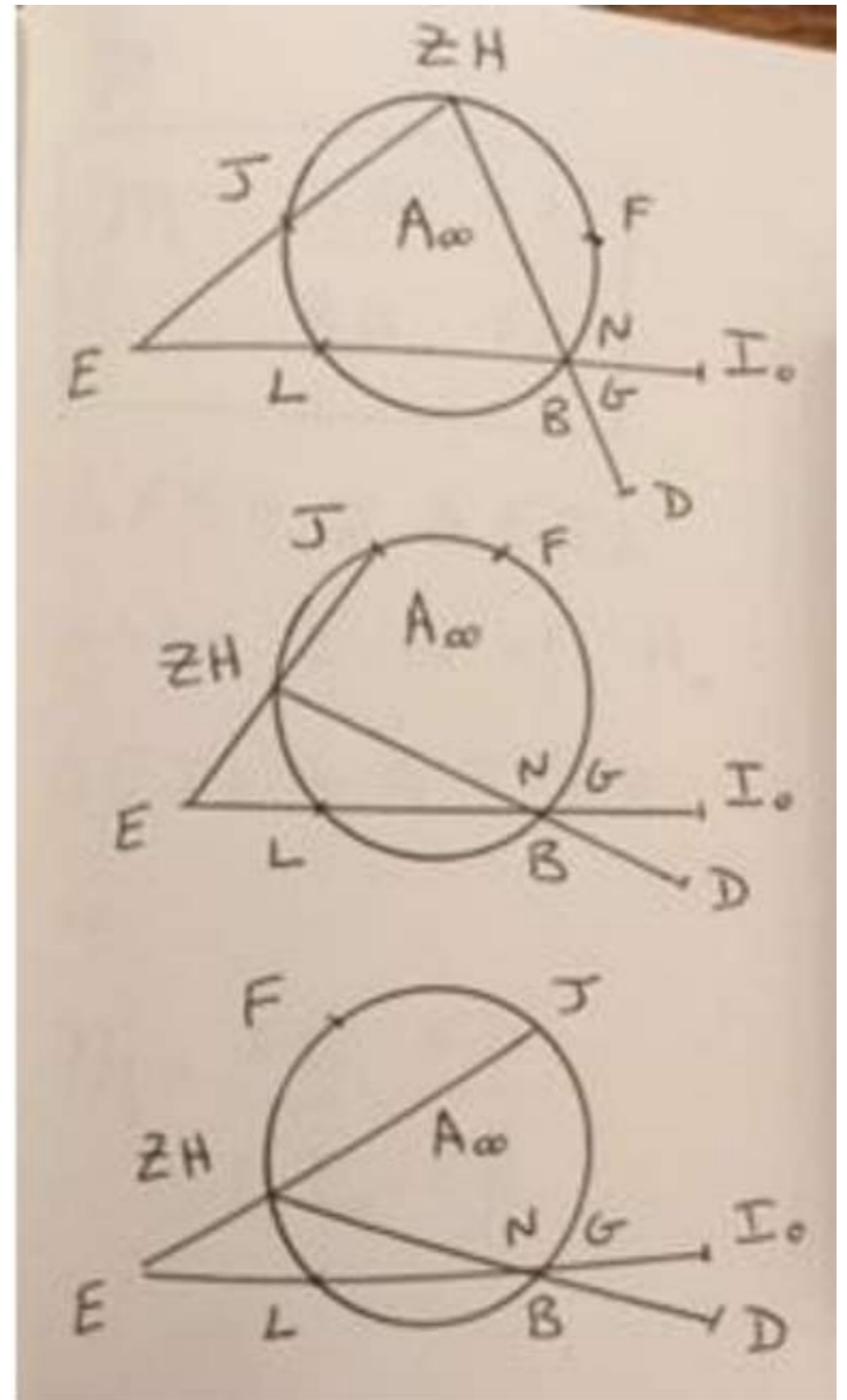


The distance correction at D:



Since the distance correction at D moves Z to H, rays leaving G after this correction must be afocal, resulting in afocal axial angular magnification equaling:

$$FD/FG (= FD/FB)$$



The (total) axial magnification of distance correction equals:

$$M = (BH/BH_0)(FD/FB)$$

$$\Delta EBH \cong \Delta EJL$$

If E is at H_o , the distance refractive error is completely due to an axial length that is not standard.

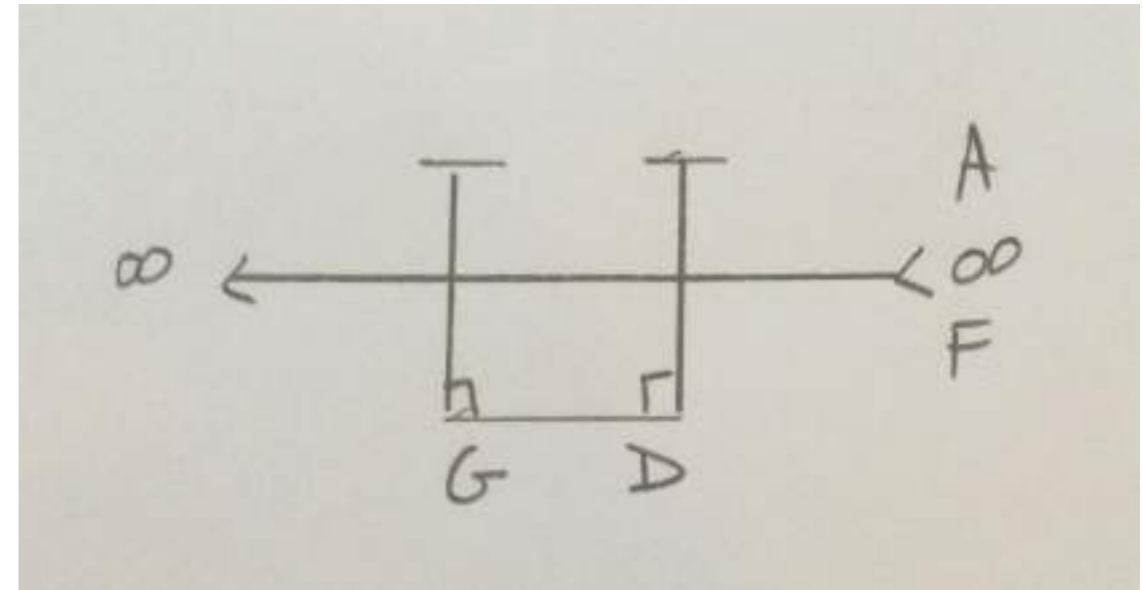
If $\Delta EJL \cong \Delta I_oFB$, then:

$$M = (FB/FI_o)(FD/FB) = FD/FI_o$$

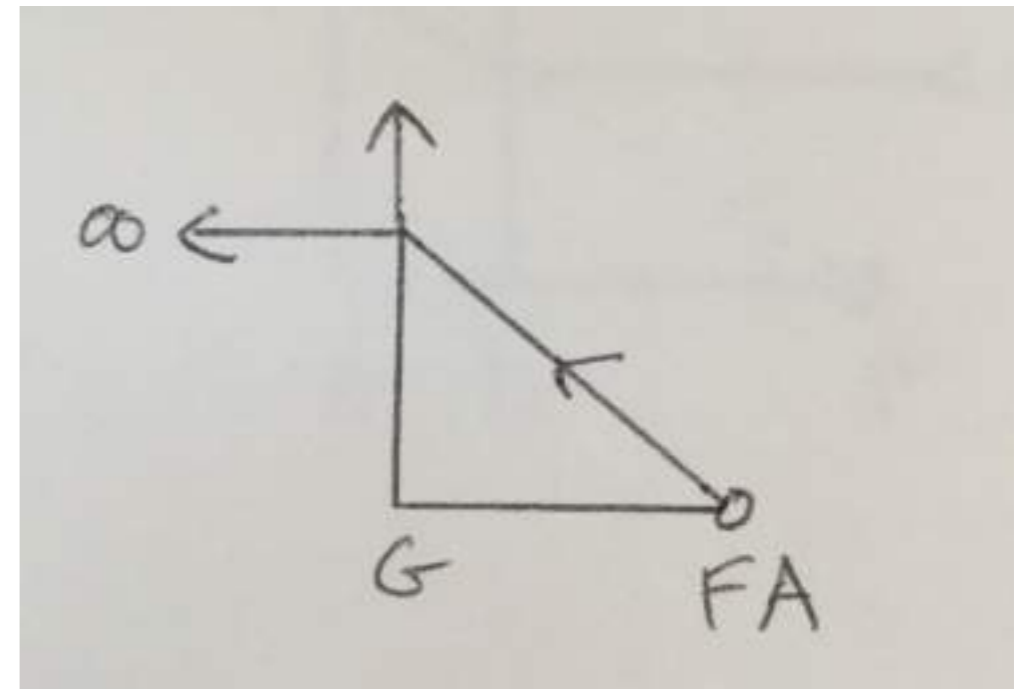
There is then no (total) axial magnification of distance correction if the correction D lies at I_o , the front focal point of the standard eye.

8). axial magnification of near correction

There is no afocal axial angular magnification FD/FB when object A is at distance with an emetropic eye. (The refractive error at G, (at B), is zero; and the focal point F of that refractive error lies at infinity).



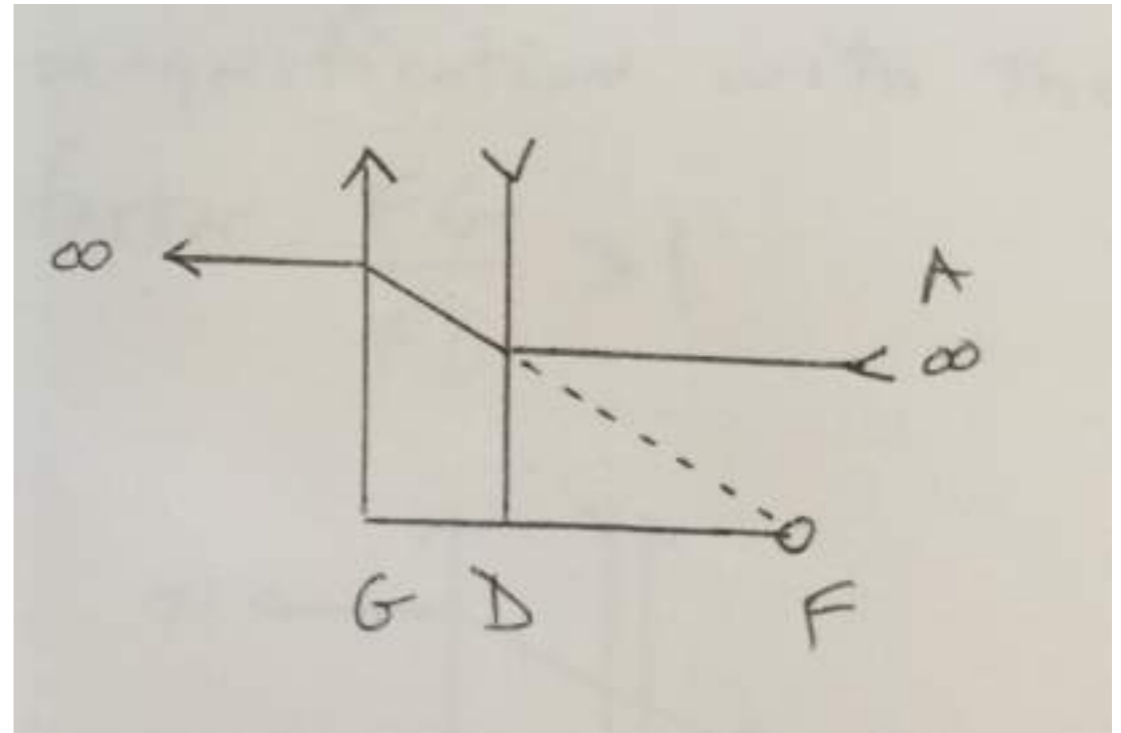
There is also no afocal axial angular magnification when object A is at the front focal point of an uncorrected myopic eye. (The system is not afocal, and involves only one refracting element).



As discussed, a distance myopic correction at D creates afocal axial angular minification:

$$FD/FG < 1$$

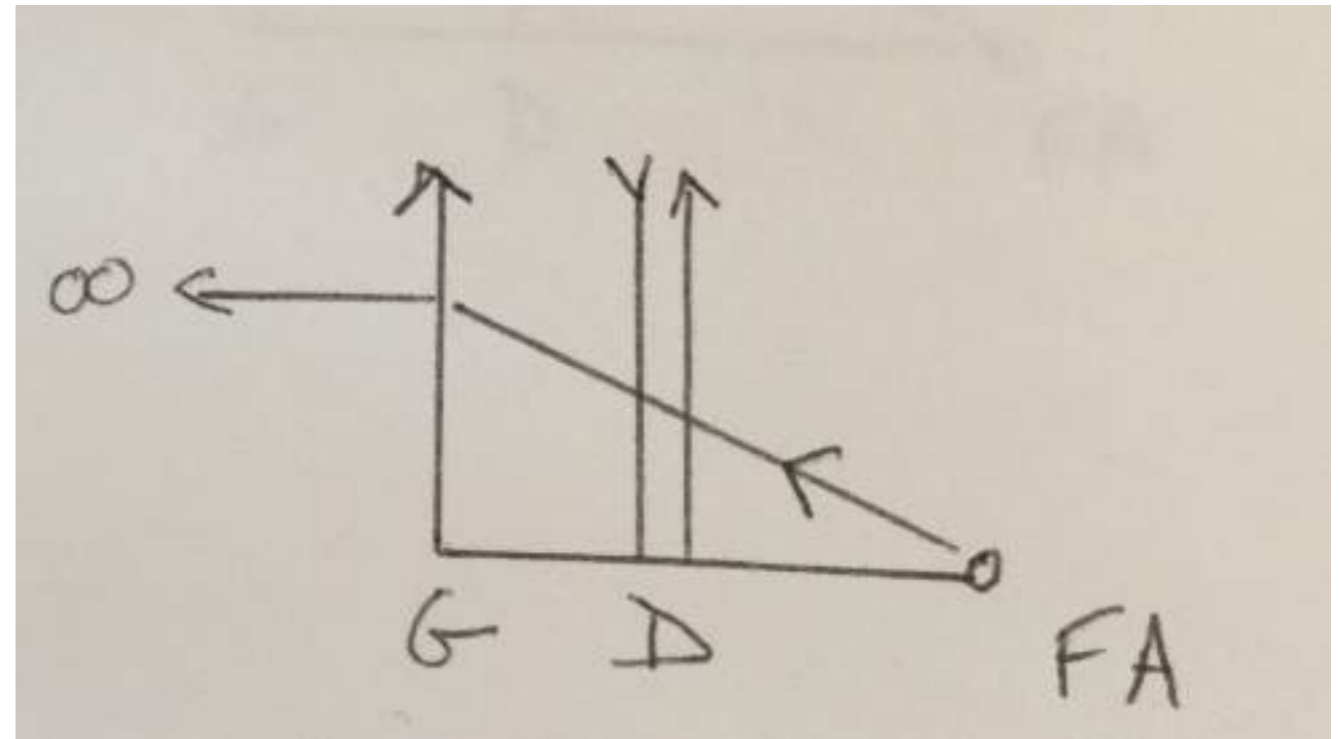
and this is relative to either the myopic eye with object A at its front focal point F, or the emmetropic eye with object A at distance.



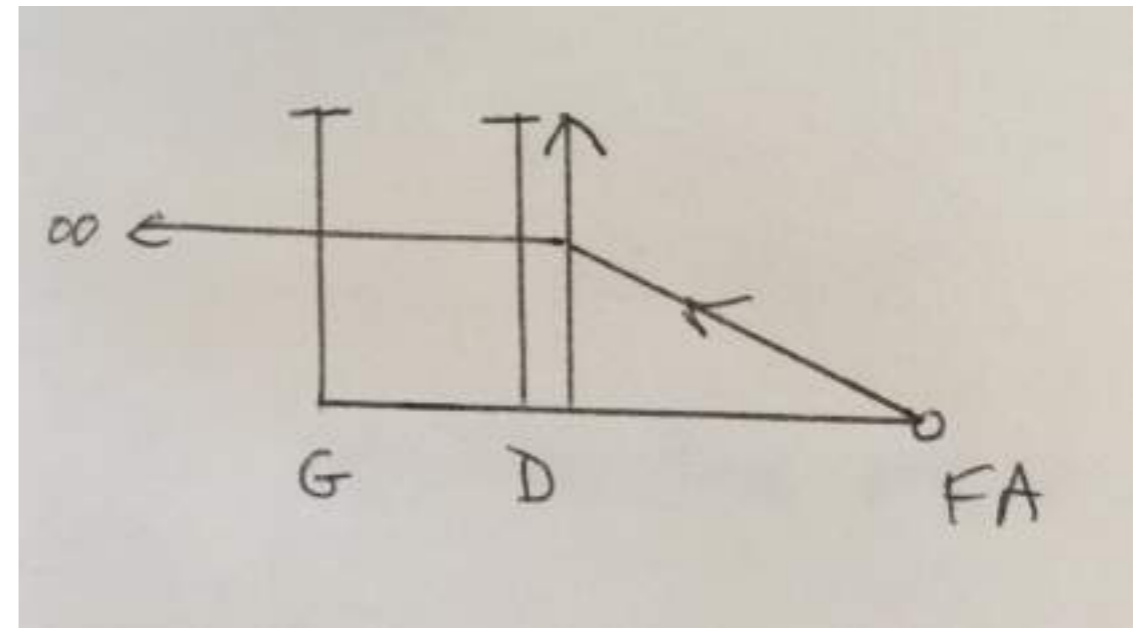
Removing the myopic distance correction at D with a converging lens at D removes this afocal axial angular magnification with the factor:

$$FG/FD > 1$$

and this magnification of near correction is relative to the distance corrected myope.



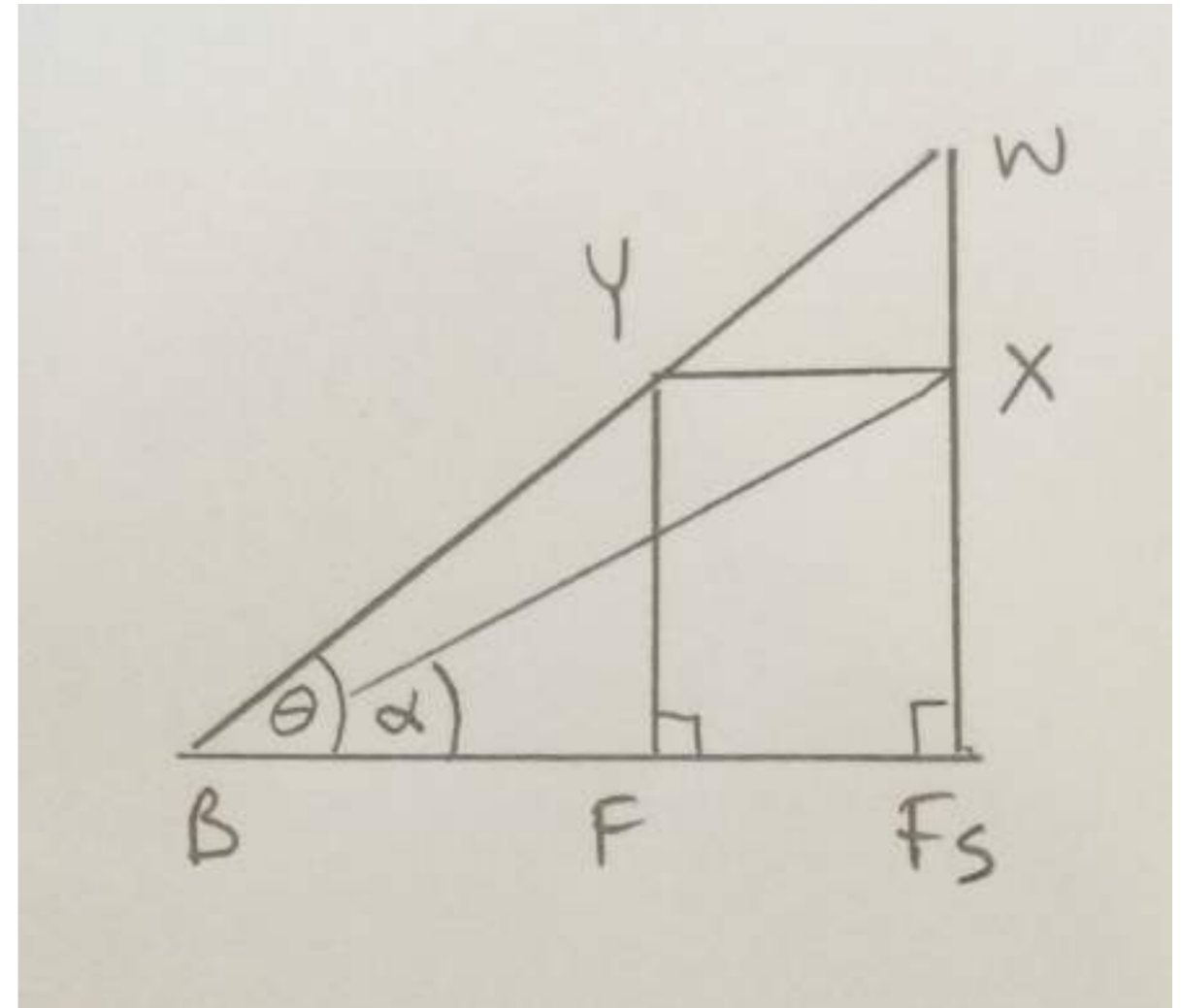
If additional converging power is added to the converging lens so that the near focal point is in focus for an *emmetropic* eye, which we then consider to be the reference eye, the magnification of near correction is still that which is removed with the factor:



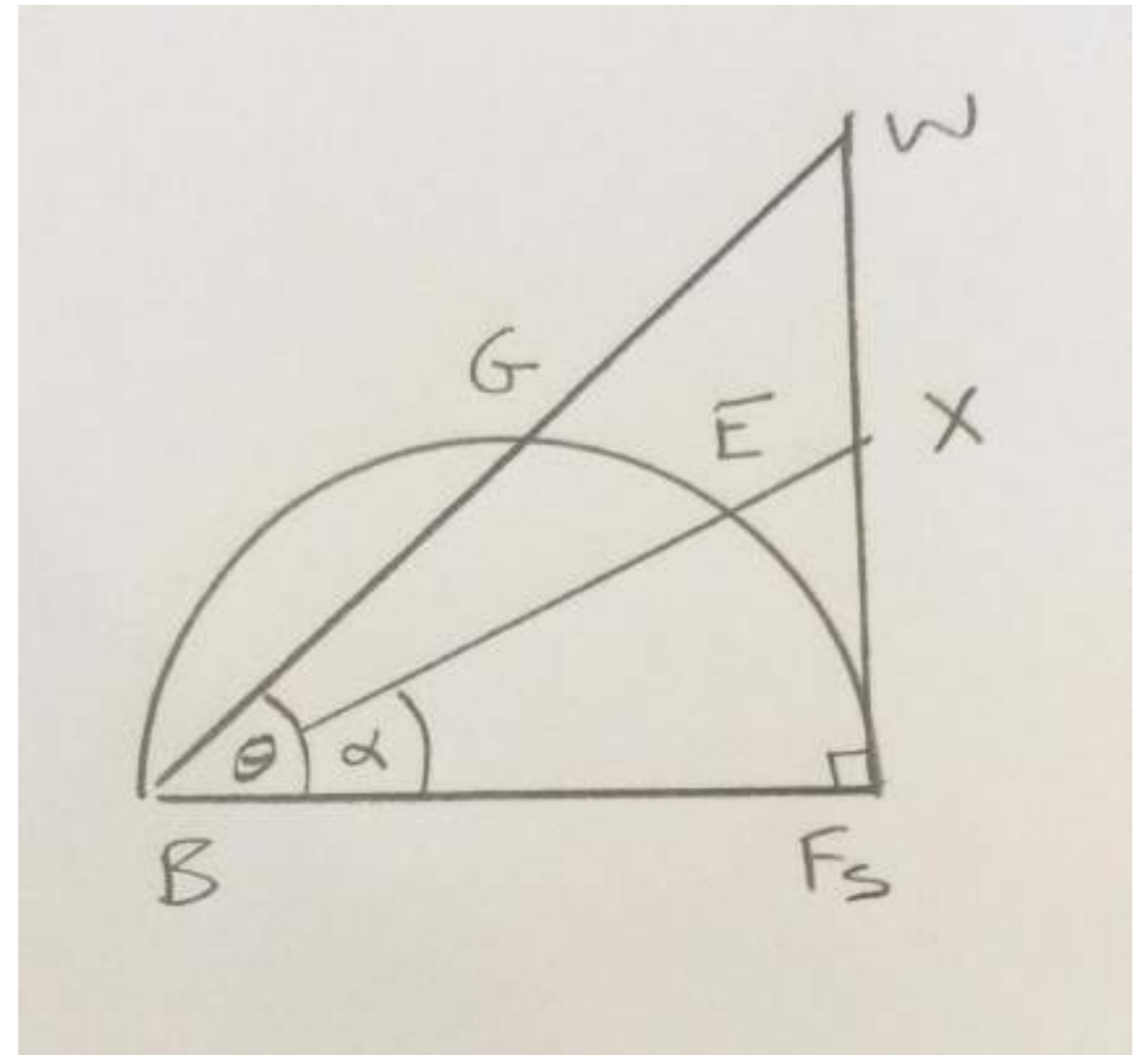
$$FG/FD > 1$$

9). object angular subtense magnification

When an object at a standard distance F_s is moved to F :



The object angular subtense magnification equals:



$$\theta/\alpha = (\sim GF_s/BF_s)/(\sim EF_s/BF_s)$$

as $XF_s \Rightarrow 0$

the object angular subtense magnification approaches its axial value:

$$\theta/\alpha \Rightarrow WF_s/XF_s = WF_s/YF = BF_s/BF$$

which equals the *axial*
object angular subtense magnification.

The ratio describing axial object angular subtense magnification:

BF_s/BF

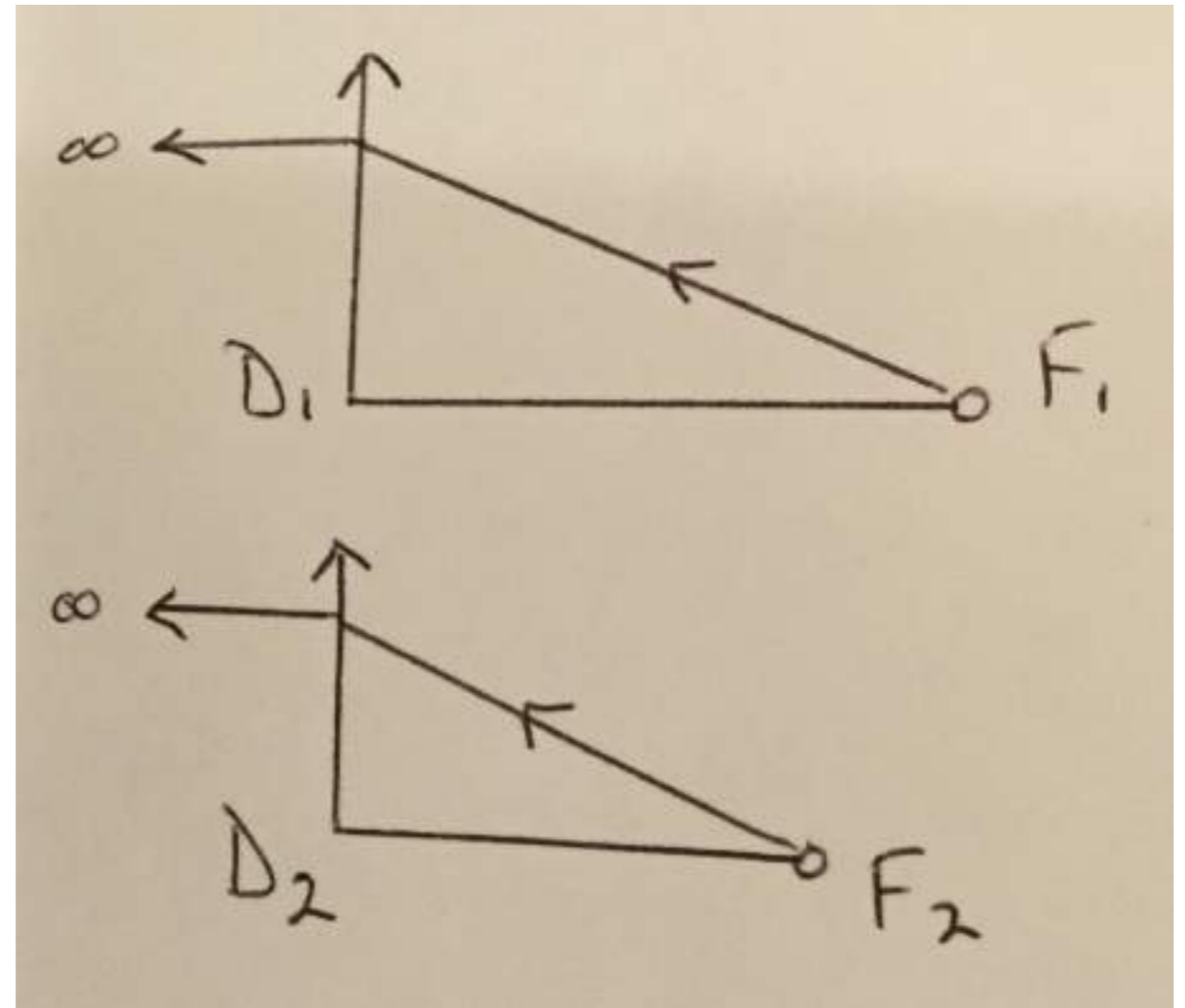
when multiplied by the ratio describing near magnification due to a single converging lens producing parallel light for an emmetropic eye:

FB/FD

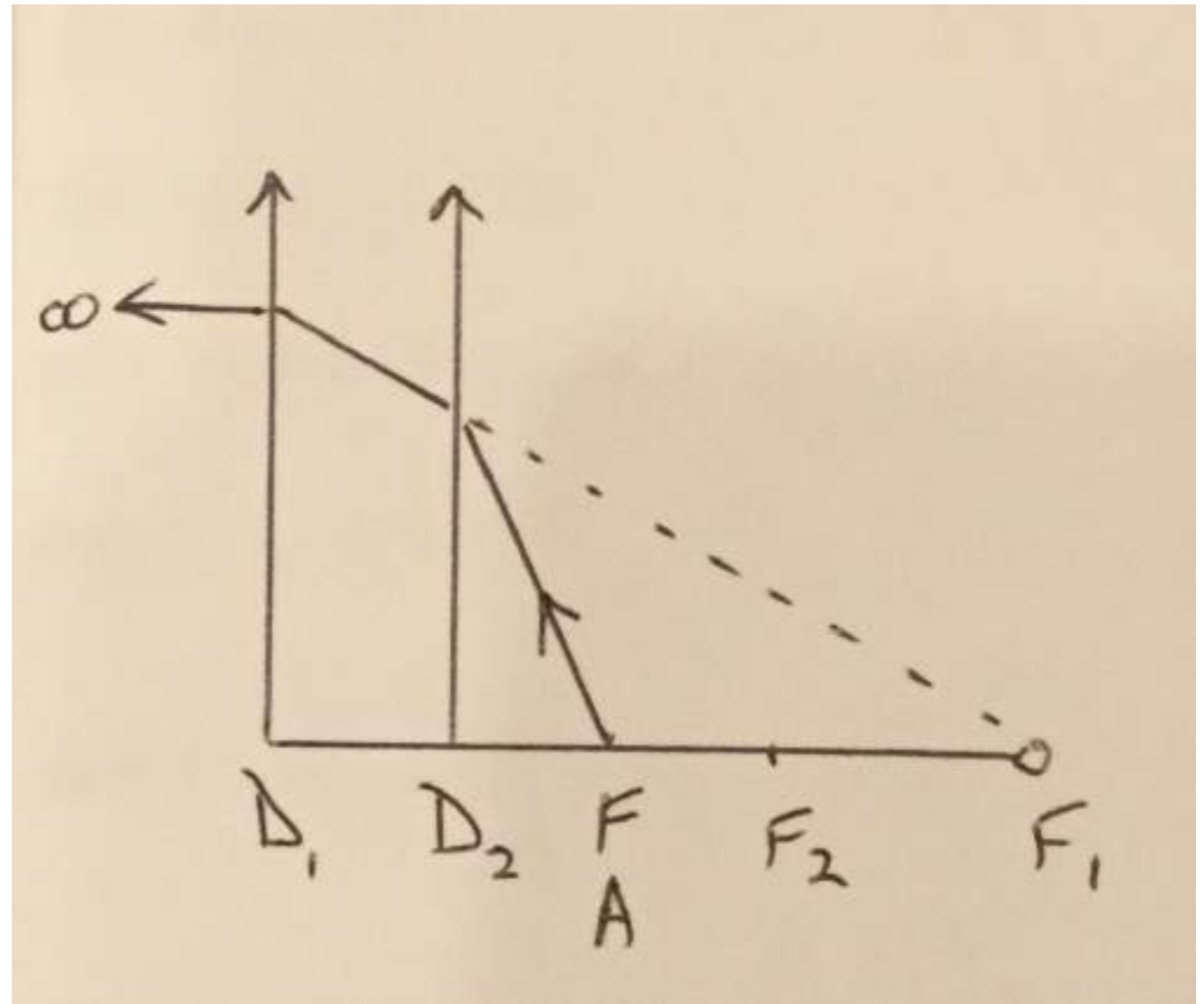
produces a ratio which factors out the object's actual distance to the eye, confirming that when a converging lens is used with its front focal point at the object, so parallel light leaves the converging lens from the object, the image size is the same regardless of the object-to-eye distance.

10). stand magnifier magnification

When the converging lens at D is split into two converging lenses:



with the same
combined
focus F :



the ratio describing axial near magnification due to a single converging lens producing parallel light for an emmetropic eye:

FB/FD

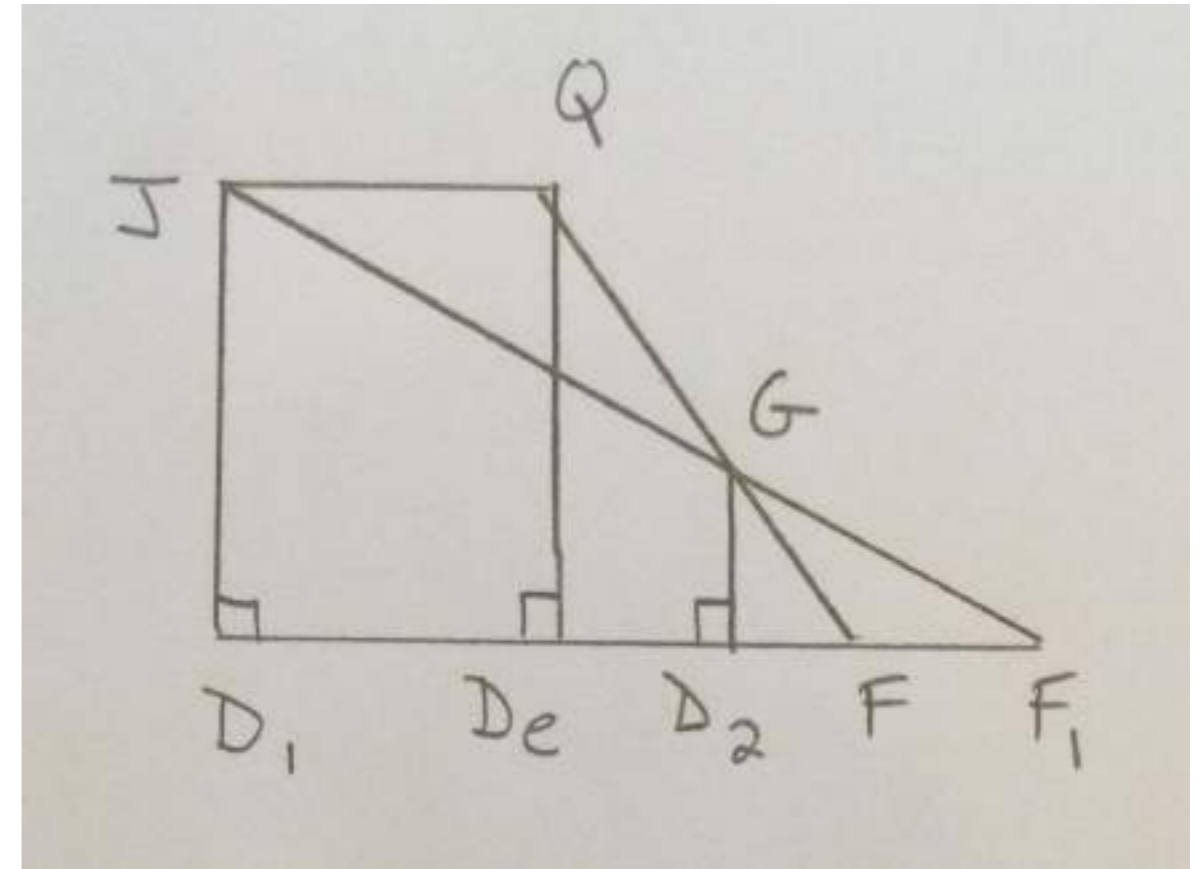
must be expressed *as if* all convergence occurred at a single unknown axial point D_e :

FB/FD_e

De can be located using triangles.

$$D_2G/D_2F = DeQ/DeF$$

$$D_2G/D_2F_1 = D_1J/D_1F_1$$



$$D_2F(DeQ/DeF) = D_2F_1(D_1J/D_1F_1)$$

$$DeQ/DeF = (D_2F_1/D_2F)(D_1J/D_1F_1)$$

$$1/DeF = (D_2F_1/D_2F)(1/D_1F_1)$$

$$FB/FDe = (D_2F_1/D_2F)(FB/D_1F_1)$$

Multiplying the axial object subtense magnification by the axial magnification of near correction (relative to the same eye without refractive error) produces:

$$\text{BFs}/\text{FDe} = (D_2F_1/D_2F)(\text{BFs}/D_1F_1)$$

The converging lens D_2 creates a virtual image F_1 of an object at F . When considering a stand magnifier with lens D_2 , constant stand height D_2F , and reading spectacle add or ocular accommodation D_1 , the stand magnifier's (constant) enlargement of the object at F equals:

$$E = D_2F_1/D_2F$$

The stand magnifier's axial magnification is its (constant) enlargement factor E , multiplied by what would be produced by D_1 alone, if the object A were at F_1 .